

## A proposed technique for determining aerodynamic pressures on residential homes

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**Abstract.** Wind loads on low-rise buildings in general and residential homes in particular can differ significantly depending upon the laboratory in which they were measured. The differences are due in large part to inadequate simulations of the low-frequency content of atmospheric velocity fluctuations in the laboratory and to the small scale of the models used for the measurements. The imperfect spatial coherence of the low frequency velocity fluctuations results in reductions of the overall wind effects with respect to the case of perfectly coherent flows. For large buildings those reductions are significant. However, for buildings with sufficiently small dimensions (e.g., residential homes) the reductions are relatively small. A technique is proposed for simulating the effect of low-frequency flow fluctuations on such buildings more effectively from the point of view of testing accuracy and repeatability than is currently the case. Experimental results are presented that validate the proposed technique. The technique eliminates a major cause of discrepancies among measurements conducted in different laboratories. In addition, the technique allows the use of considerably larger model scales than are possible in conventional testing. This makes it possible to model architectural details, and improves Reynolds number similarity. The technique is applicable to wind tunnels and large scale open jet facilities, and can help to standardize flow simulations for testing residential homes as well as significantly improving testing accuracy and repeatability. The work reported in this paper is a first step in developing the proposed technique. Additional tests are planned to further refine the technique and test the range of its applicability.

**Keywords:** aerodynamics; atmospheric surface layer; building technology; low-rise structures; open jet facilities; residential buildings; wind engineering; wind tunnels.

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### 1. Introduction

High winds cause the largest losses due to natural disasters in the U.S. Annual losses due predominantly to high winds from hurricanes alone averaged on the order of \$10 billion from 1990-1995. Low-rise buildings such as single-family residences and small commercial structures, which constitute over 70% of the U.S. building stock, account for a majority of these losses. The reduction of these losses requires the development of appropriate design and retrofitting provisions for such buildings, which currently are limited due to aerodynamic measurement difficulties in the current

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state of the art. An international round-robin set of wind tunnel tests of low-rise structures conducted at six reputable laboratories showed that wind-induced internal forces in structural frames, and pressures at individual taps, can differ from laboratory to laboratory by factors larger than two (Fritz *et al.* 2008). This variation is a barrier to the development of rational building standards. Owing in part to such differences aerodynamic pressures on low-rise structures specified in the ASCE 7 Standard (ASCE 7-2005) can be smaller by as much as 50% than those measured in the wind testing laboratories or specified in the literature (Surry *et al.* 2003, StPierre *et al.* 2005, Ho *et al.* 2005, Coffman *et al.* 2009).

Among the reasons for the non-repeatability of conventional tests across laboratories are two facts. First, the low-frequency fluctuations of the oncoming flow turbulence in the atmospheric surface layer are difficult to simulate in the laboratory, and second, the techniques for their production in the laboratory are not standardized. Since those fluctuations contain the bulk of the turbulent energy, they contribute overwhelmingly to the turbulence intensity and the integral turbulence scale.

For large buildings, imperfect spatial coherence of atmospheric flows results in significant reductions of the overall wind effects with respect to the case of perfectly coherent flows. However, the smaller the building dimensions, the smaller are those reductions. In particular, the reductions can be expected to be small for residential homes. It is hypothesized that peak aerodynamic effects experienced by a small building subjected to flows whose velocities have significant low-frequency fluctuations (hereinafter called “*atmospheric boundary layer-type or ABL-type flows*”) are not substantially different from those induced by flows hereinafter called “*simplified flows*”; that is, for flows for which (a) the low-frequency content is negligible, while (b) the mean velocities are larger than their counterparts in atmospheric boundary layer flows by amounts that make up for the absence of low-frequency fluctuations.

The objective of the proposed technique is to achieve flow simulations aimed to determine aerodynamic pressures on residential homes that are more effective from the point of view of testing accuracy and repeatability than is the case for conventional simulations in most wind testing facilities, including wind tunnels (Cermak 1995) and large scale open jet facilities (Huang *et al.* 2009, Bitsuamlak *et al.* 2009, Bitsuamlak *et al.* 2010, Gan Chowdhury *et al.* 2009, Masters and Lopez 2010, Smith *et al.* 2010). The approach for achieving this goal is the following. No attempt is made to simulate low-frequency components, i.e., components with non-dimensional frequencies  $nz / U(z)$  less than say, 0.1 or 0.2, for which it is commonly accepted that inertial subrange assumptions are no longer applicable ( $n$  = frequency,  $z$  = height above the surface,  $U$  = mean wind speed of the turbulent flow averaged over, say, 10 min or 1 hour) (Fichtl and McVehil 1970). Rather, the mean speed of the laboratory flow is augmented from  $U(z)$  to  $cU(z)$ , where  $c > 1$  is determined as shown in the Appendix. Note that the vertical profile of the simulated flow speeds  $U(z)$  and  $cU(z)$  is the same. This approach amounts in effect to substituting for the low-frequency fluctuations of the flow with mean speed  $U(z)$  an incremental speed  $(c-1)U(z)$  constant in time. This incremental speed may be viewed as a conceptual flow fluctuation with vanishing frequency (i.e., with infinite period). The spatial coherence for this conceptual fluctuation is unity. Methodology for the determination of factor  $c$  is described in the Appendix.

In addition to eliminating a cause of discrepancies among measurements conducted in different laboratories, the proposed approach allows the use of considerably larger model scales than are possible in conventional testing, since it eliminates restrictions imposed by integral turbulence scales achievable in the laboratory.

Provided that the spatial separations are of the order of, say, 20 m or less, for the low-frequency components of the atmospheric flow fluctuations, the spatial coherences are relatively large. This is shown in the Appendix by using the expression for spatial coherence (Vickery 1970)

$$Coh(r, n) = e^{-f} \quad (1)$$

$$f = \frac{n[C_z^2(z_1 - z_2)^2 + C_y^2(y_1 - y_2)^2]^{1/2}}{\frac{1}{2}[U(z_1) + U(z_2)]} \quad (2)$$

where  $n$  is the frequency of atmospheric flow fluctuations,  $U(z)$  is the mean wind speed at height  $z$ ,  $y_1, y_2$  and  $z_1, z_2$  are horizontal and vertical coordinates of points  $M_1$  and  $M_2$  (the distance between which is denoted by  $r$ ), and the line  $M_1, M_2$  is assumed to be perpendicular to the direction of the mean wind speed.  $C_y$  and  $C_z$  are exponential decay coefficients that are determined experimentally. The proposed testing procedure for low-rise buildings is based on the hypothesis that the spatial coherences of interest are indeed sufficiently large.

To test the hypothesis that peak aerodynamic effects experienced by a small building subjected to ABL-type flows are not substantially different from the aerodynamic effects induced by simplified flows, two sets of tests were carried out as follows. One set of tests used a model of the Silsoe building (Murakami and Mochida 1990, Richards *et al.* 2001), while the second set used a model of the Texas Tech University (TTU) test building (Okada and Ha 1992). Each set of tests was based on two types of flow. The ABL-type flow was simulated by imparting to the fans quasi-periodic rotations induced by a quasi-periodic waveform signal (for details see Huang *et al.* 2009). The simplified flow contained negligible low-frequency fluctuations (substituting for the low-frequency fluctuations an incremental speed  $(c-1)U(z)$  constant in time), as explained earlier. A methodology for estimating the factor  $c$  is presented in some detail in the Appendix. As is shown subsequently in the section “Results”, the pressure measurement results obtained under these two types of flows support the hypothesis on which this paper is based.

## 2. Description of tests

The experiments were carried out by utilizing the 12-fan small-scale Wall of Wind (WoW) (Fu *et al.* 2010, Gan Chowdhury *et al.* 2010), an open jet test facility at Florida International University (Fig. 1). Two specimens were built as follows

- (1)  $8.9 \times 8.9 \times 8.9$  cm ( $3.5 \times 3.5 \times 3.5$  in) Silsoe cube (length scale being 1:67.5)
- (2)  $17.5 \times 26.0 \times 7.7$  cm ( $6.89 \times 10.24 \times 3.03$  in) TTU building (length scale being 1:52)

High frequency cobra probes were used for wind speed measurements and set at 625 Hz sampling rate. A 64 channels pressure transducer was used at a 100 Hz sampling rate. For specimens (1) and (2), all the pressure taps were distributed over the external surface, covering the windward, roof, leeward, and side walls as shown in Fig. 2. Pressures were measured for wind angles of attack of  $0^\circ$  and  $45^\circ$ .

Two types of wind flows were generated to simulate the wind stream without and with low



Fig. 1 Small-scale 12-fan Wall-of-Wind (WoW)

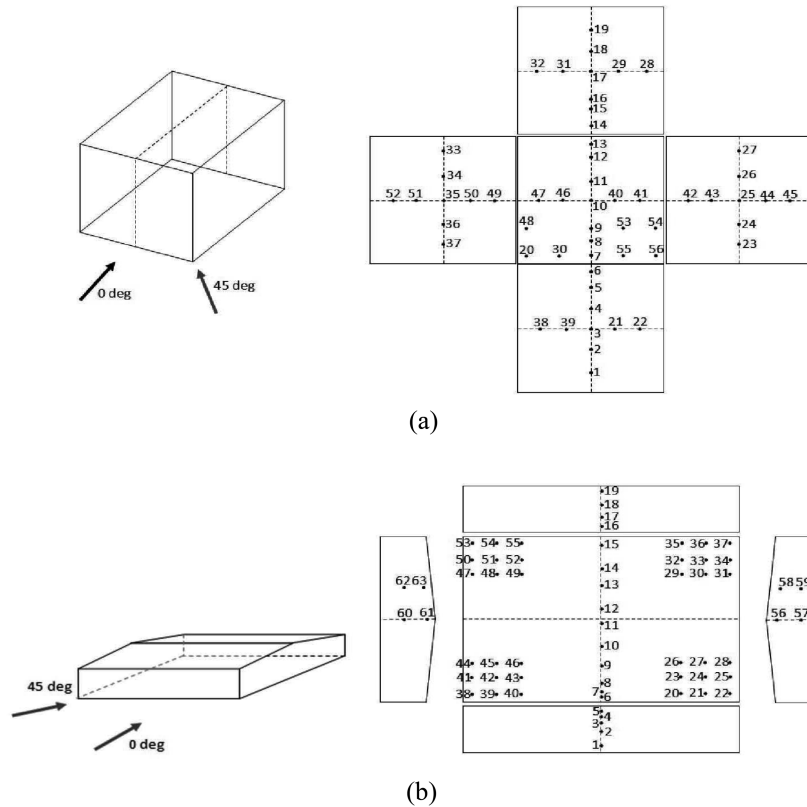


Fig. 2 Tap layout for the two test specimens: (a) 8.9 x 8.9 x 8.9 cm Silsoe Cube and (b) 17.5 x 26.0 x 7.7 cm TTU Building

frequency turbulence. To simulate the wind flow without low frequency turbulence components, a flat waveform signal was input into the WoW controller. To simulate the wind flow with low frequency components, a quasi-periodic waveform signal was input into the WoW controller, based on the spectrum of the longitudinal velocity fluctuations for real hurricanes (Yu *et al.* 2008). The

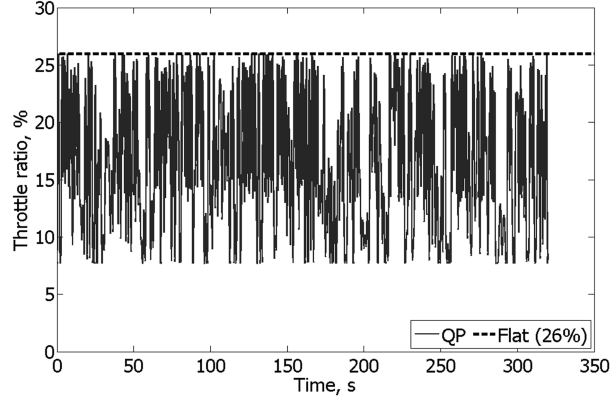


Fig. 3 Input waveforms of flat flow (without low-frequency content) and quasi-periodic (QP) flow (with low-frequency content)

waveform generation details are described in Huang *et al.* (2009). Fig. 3 presents the input waveforms for generating the airflows without and with low-frequency turbulence. The peak of the input signal for the quasi-periodically driven fans (generating ABL-type flows) was equal to the constant input signal for the uniformly driven fans (generating simplified flows). Simplified estimation of increased mean wind speed  $c'U(z)$  (for uniform flow) was estimated by using Step 4, variant (b), of the Appendix. To ensure stability and repeatability of the peak pressure values, all the tests were carried out for 5 min. For the TTU model this duration corresponds at full scale to 90 min, as shown by Eqs. (3) and (4)

$$\frac{T_p U_p}{L_p} = \frac{T_m U_m}{L_m} \quad (3)$$

$$T_p = \left( \frac{L_p}{L_m} \right) \left( \frac{U_m}{U_p} \right) T_m = (52) \left( \frac{16.9(m/s)}{50(m/s)} \right) \times 5(\text{min}) = 87.9 \text{ mm} \quad (4)$$

where  $T$ ,  $U$ , and  $L$  are the time, mean wind speed, and characteristic length, respectively, and the subscript  $p$  and  $m$  refer to the prototype and the model, respectively. The length scale of 1:52 was based on the scale of the TTU model and the full-scale wind speed is considered as 50 m/s. For the quasi-periodic flow the mean wind speed was 16.9 m/s. For the Silsoe model the 5 min. duration corresponded to about 2 hrs at full-scale.

To simulate atmospheric boundary layer (ABL) wind profiles, a passive device was used to generate the vertical profile of wind flows (Gan Chowdhury *et al.* 2010). This device consisted mainly of a set of planks. The inclination of each plank was adjusted by trial and error to ensure that the mean speeds of the air flow match reasonably well the mean flow in typical open terrain (power law exponential  $\bar{\alpha} = 1/6$  pertaining to mean flow, see Fig. 4).

The measured turbulence intensity at 89 mm (3.5 in) above ground (corresponding to the roof height of the Silsoe model) was about 6% for the flat flow and 26% for the quasi-periodic flow. Mean wind speeds were 24.8 m/s and 16.9 m/s for the flat and quasi-periodic flows, respectively. This ensured that the flow with negligible low-frequency content had a mean velocity equal to the sum, in the flow with significant low-frequency content, of (a) the mean velocity, and (b) the peak fluctuating velocity induced by the low-frequency fluctuations. The optimal distance between the

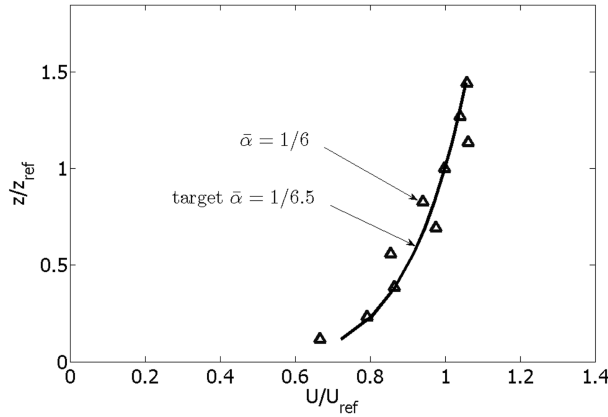


Fig. 4 Mean wind speed profile

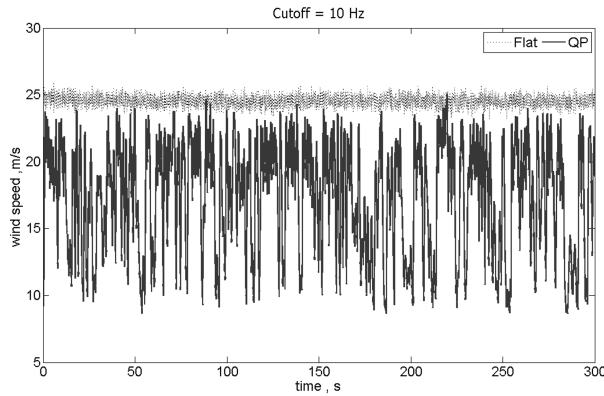


Fig. 5 Time history of flat flow (without low-frequency content), and quasi-periodic (QP) flow (with Low-Frequency Content)

exit of the WoW and the windward wall surface of the test models was 22.0 cm (8.6 in). Fig. 5 shows the wind velocity time histories of the flows without and with low-frequency components. Fig. 6 shows the dimensional spectra for both flows. For comparison purposes the figure also shows the spectrum proposed by Yu *et al.* (2008) for hurricane wind data in open terrain exposure, obtained within the framework of the Florida Coastal Monitoring Program (Masters 2004) [mean wind speed of 16.9 m/s, turbulence intensity of 26%, and parameter  $\beta = 6.0$  (Simiu and Scanlan 1996)]. The spectrum for the flat flow shows significantly lower ordinates than those of the FCMP spectrum. The spectrum for the flow with low-frequency fluctuations (i.e., the quasiperiodic flow) has ordinates comparable to those of the FCMP spectrum for the interval of  $n = 0.03$  Hz to  $n = 1$  Hz. The small-scale fans were not capable of producing significant fluctuations beyond  $n = 1$  Hz, hence the deficit in the quasiperiodic flow spectrum ordinates beyond  $n = 1$  Hz.

Because of the limitations of the small scale WoW fan's performance, it was possible to obtain spectra covering only the dimensional interval  $n = 0.03$  Hz to  $n = 10$  Hz, that is, the non-dimensional interval up to  $f = 0.06$ . The turbulence intensities achieved in the experiments increased from 6% in the absence of low-frequency fan rotations to 26% when quasiperiodic fan rotations were activated. The results of the experiments presented in the paper show that the effect of

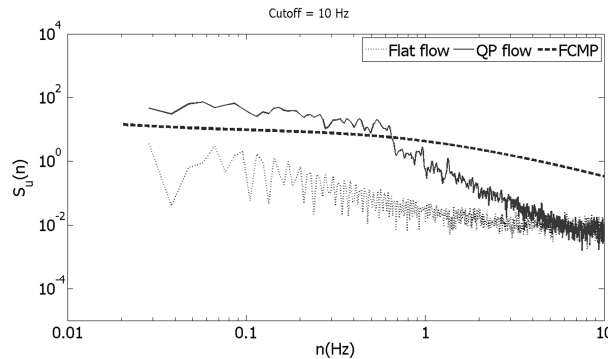


Fig. 6 Dimensional spectra of longitudinal wind flow fluctuations

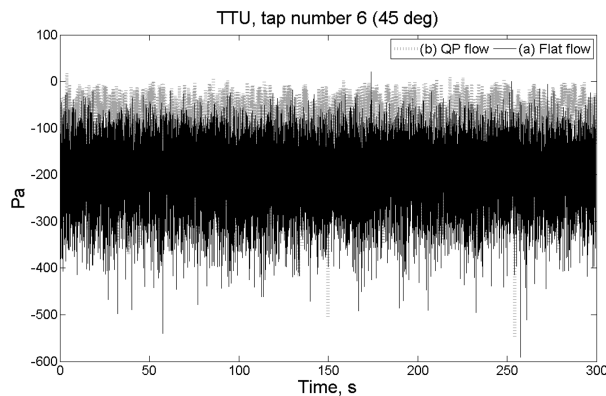


Fig. 7 Typical roof pressure time history data under (a) flat wind flow and (b) quasi-periodic (QP) wind flow

increments in the mean speeds (i.e., the effect of incremental “zero frequency” fluctuations) was a reasonable substitute for the effect of low-frequency fluctuations. This was the case not only for the aerodynamics of the windward face of the structure, but also for the aerodynamics of the structure as a whole. Quantitative experimental information (a) corresponding to other non-dimensional frequency intervals and (b) on the sizes of the windward face for which the assumption of perfect coherence of the oncoming low-frequency fluctuations is not overly conservative, will require large-scale WoW testing used in conjunction with analytical calculations in which the parameters of the flow coherence are based on measurements of the large-scale turbulent flow.

### 3. Results

Typical time histories of roof pressures are shown in Fig. 7. The observed peaks can exhibit wide variability from one realization to another due to their random nature. To remove the uncertainties inherent in the randomness of the peaks, probabilistic analyses were performed using the procedure developed by Sadek and Simiu (2002) ([www.nist.gov/wind](http://www.nist.gov/wind)) for obtaining statistics of pressure peaks from observed pressure time histories. Because estimates obtained by this procedure are based on the entire information contained in the time series, they are more stable than estimates based on

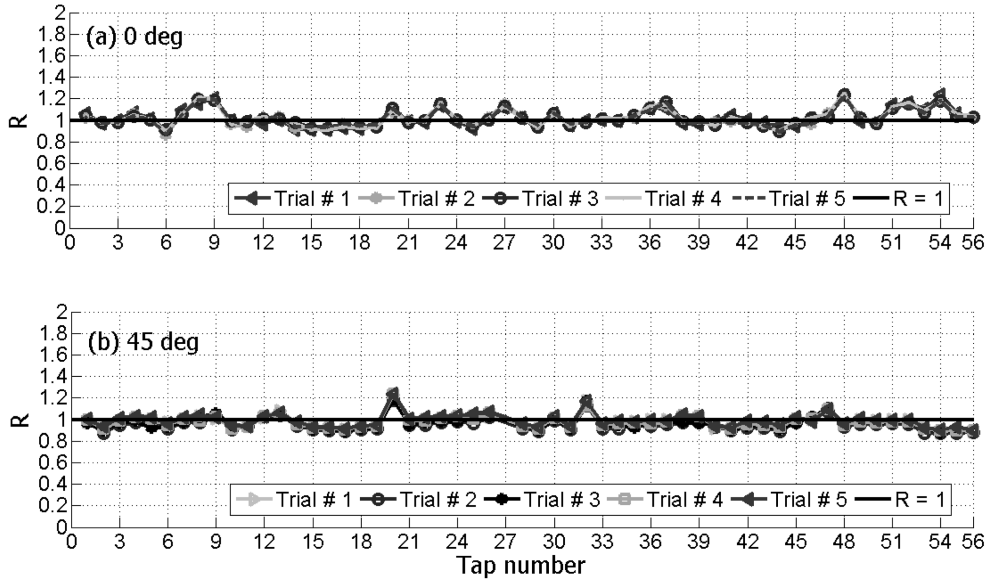


Fig. 8 Peak pressure ratio for flat to quasi-periodic (QP) flows vs. tap number (silsoe cube)

Table 1 Mean and standard deviation of the ratio  $r$  obtained for five repeated tests with the silsoe cube model for two wind azimuths

Azimuth	Ratio	Tap # 5	Tap # 7	Tap # 14	Tap # 49	Tap # 56
0 deg	$R_{\text{mean}}$	1.0092	1.0650	0.9439	1.0166	1.0308
	$R_{\text{std}}$	0.0028	0.0164	0.0257	0.0148	0.0021
45 deg	$R_{\text{mean}}$	0.9796	0.9946	0.9557	0.9854	0.8907
	$R_{\text{std}}$	0.0391	0.0228	0.0160	0.0198	0.0070

observed peaks and provide a clearer and more meaningful basis for the comparisons. The comparisons were in all cases based on the 95<sup>th</sup> percentile of the estimated distributions of the peaks.

Fig. 8 shows the ratio ( $R$ ) of the 95<sup>th</sup> percentile estimates of peak pressures measured for the Silsoe model under flow with no low-frequency content to peak pressures measured with low frequency content. The experiments were repeated 5 times. As the results show, the ratios are typically close to unity. In a few cases they are higher than unity by approximately 20% and lower than unity by approximately 17%.

Table 1 lists means and standard deviations of the ratio  $R$  obtained for each of the selected taps on the Silsoe model for two wind azimuths ( $0^\circ$  and  $45^\circ$ ) in five repeated tests. Taps were chosen to represent windward wall, roof, leeward wall, top corner, and side walls. Results show that the mean value of the ratio  $R$  for the five trials is also close to one. Low standard deviation values indicate that the repeatability of the tests is satisfactory.

Fig. 9 shows peak pressure ratios for TTU model. The largest ratio  $R$  at the roof is about 20% higher than unity. Table 2 lists mean and standard deviation of the ratio  $R$  obtained for five repeated tests with the TTU model for two wind azimuths ( $0^\circ$  and  $45^\circ$ ). Arbitrary taps were chosen to represent windward, roof, leeward, top corner, and side wall. Results show that the mean value of



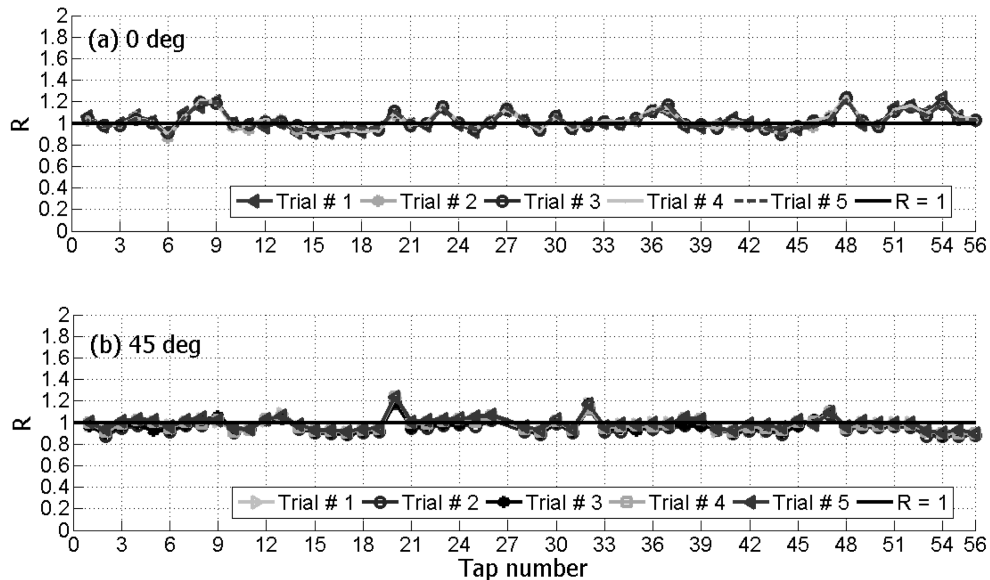


Fig. 9 Peak pressure ratio for flat to quasi-periodic (QP) flows vs. tap number (TTU model)

Table 2 Mean and standard deviation of the ratio  $r$  obtained for five repeated tests with the TTU test model for two wind azimuths

Azimuth	Ratio	Tap # 4	Tap # 8	Tap # 16	Tap # 38	Tap # 60
0 deg	$R_{\text{mean}}$	1.0060	1.1528	0.9607	1.2052	0.9786
	$R_{\text{std}}$	0.0191	0.0338	0.0230	0.0235	0.0107
45 deg	$R_{\text{mean}}$	1.0017	0.9773	1.0260	0.8384	1.0320
	$R_{\text{std}}$	0.0271	0.0218	0.0210	0.0059	0.0117

the ratio,  $R$ , for the five trials is close to one. The standard deviations of the results are in all cases small. This establishes the repeatability of the tests performed in accordance with the procedure proposed in this paper.

Future tests are planned in FIU's large-scale 12-fan WoW facility currently under construction, with a view to validating the proposed procedure for a wide range of model-to-full-scale ratios. For these tests, attendant skewness and kurtosis calculations will be performed to determine possible deviations of the distributions from normality.

#### 4. Conclusions

Flows that attempt to simulate low-frequency fluctuations for the testing of residential homes and other low-rise buildings or portions thereof have the following drawbacks. First, they tend to induce significant errors in the estimation of the pressures. These errors are typically much larger than errors inherent in the use of flows with no low-frequency fluctuations, and affect adversely the repeatability of the tests. To achieve better agreement among results across different laboratories, a standard flow simulation protocol for low-rise buildings will have to be developed for both wind

tunnels and large scale open jet facilities. The standardized flow simulations will result in improved testing accuracy and repeatability for residential homes.

Second, the simulation of low-frequency turbulent fluctuations imposes severe constraints on the geometric model scale, which unavoidably entail additional errors in the estimation of aerodynamic effects. For flows with no low-frequency fluctuations these constraints are eliminated, the only subsisting constraints on model scale being those associated with blockage.

The results of the tests presented in this paper support the hypothesis that flows with no low-frequency content that simulate correctly the mean wind profile in the atmospheric boundary layer are adequate for the simulation of pressures induced by atmospheric flows on low-rise buildings with dimensions comparable to those of individual homes. The errors inherent in such flows are far smaller than those that can occur in conventional wind tunnel tests. The proposed technique allows the use of larger test models allowing the modeling of architectural details, Reynolds number improvements enhancing aerodynamic accuracy, and higher spatial resolution of pressure measurements. The work reported in this paper is viewed as a first step in developing the proposed technique.

Future tests are planned to further refine the technique and validate it for a wide range of model-to-full-scale ratios. For these tests, attendant skewness and kurtosis calculations will be performed to determine possible deviations of the distributions from normality.

The principle of the methodology is applicable not only to the proposed experimental technique but to Computational Fluid Dynamics (CFD) calculations as well. Such application would have the considerable advantage of simplifying the simulation of the oncoming flow, whose conventional representation, entailing as it does fluctuations with imperfectly correlated low-frequency fluctuations, is a major barrier to the performance of effective numerical computations.

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## Appendix. Determination of factor $c$

This Appendix proposes an answer to the question: how large should the increment of the mean velocity be in order to provide a correct approximate substitute for the missing low-frequency fluctuations?

Consider the simple case of the total wind force acting on the windward face of a rectangular building acted upon by wind normal to that face. For this case it is possible to calculate approximately that force both for flow nominally conforming to the conventional ABL model, and for flow conforming to the simplified model described earlier. The study also proposes an answer to the following question: what is the definition of “low-frequency fluctuations?” The answers based on the present study are intended to provide guidance required for aerodynamic testing of small buildings in simplified flows.

The wind speed  $U(y, z, t)$  is assumed to vary with time  $t$ , width  $y$ , and height  $z$ , and consists of the mean wind speed  $U(z)$  and the wind speed longitudinal fluctuations about the mean,  $u(y, z, t)$ . The velocity  $U(y, z, t)$  is assumed to be normal to the wider face of the building.

The objective is to create a simplified flow such that the peak total aerodynamic force  $F_{peak}$  it induces on the windward face of a building is approximately equal to the peak force induced by the ABL-type. The calculations entail the following steps:

Step 1: Estimation of peak force  $F_{peak}$  induced by the ABL flow on the windward building face:

The calculation of the peak total aerodynamic force  $F_{peak}$  is performed here under the following assumptions:

1. The spectral density of the longitudinal flow fluctuations  $u$  is described by the expression for the modified Kaimal spectrum

$$\frac{nS_u(z, n)}{u_*^2} = \frac{200f}{(1 + 50f)^{5/3}} \quad (A1)$$

where  $f$  is the reduced frequency defined as  $nz / U(z)$  and  $u_*$  is the friction velocity (Simiu and

Scanlan 1996). This expression is valid for frequencies  $0 < f \leq f_c$  in which it is reasonable to assume a cut-off frequency  $f_c = 10$  (i.e.,  $S_u(z, n) = 0$  for  $f > f_c$ ). If appropriate, different expressions for the spectrum may be employed.

2. The expression for the spatial coherence of the longitudinal wind velocity fluctuations  $u$  is given by Eqs. (1) and (2).

3. The longitudinal flow fluctuations and the flow-induced forces on the windward wall are approximately Gaussian.

Using these assumptions, the total wind-induced peak force  $F_{peak}$  on the windward wall can be expressed as the sum of the mean force and the peak force due to all fluctuations

$$F_{peak} \approx F_U + \kappa_{Fp} \sigma_{Fp} \quad (A2)$$

where

$$F_U = \int_0^h \int_0^b \frac{1}{2} \rho C_p U^2(z) dy dz \quad (A3)$$

$b$  is the width of the building,  $h$  is the height,  $\rho$  is the air density,  $C_p = P(z) / \left[ \frac{1}{2} \rho U^2(z) \right] \approx 0.8$  is the mean pressure coefficient where  $P(z)$  is the mean pressure at height  $z$ ,  $\kappa_{Fp}$  is the peak factor, and  $\sigma_{Fp}$  is the r.m.s. of the fluctuating force  $F'$ .

The peak factor for a flow with a duration of  $T$  seconds is approximately (Davenport 1964)

$$\kappa_{Fp} \approx \sqrt{2 \ln(v_{Fp} T)} + \frac{0.577}{\sqrt{2 \ln(v_{Fp} T)}} \quad (A4)$$

$$\text{where } v_{Fp} = \left[ \frac{\int_0^{n_c} n^2 S_{Fp} dn}{\int_0^{n_c} S_{Fp} dn} \right]^{1/2}$$

where  $v_{Fp}$  is the expected frequency for the peak force, and  $n_c$  is the dimensional cut-off frequency corresponding to  $f_c$ ,  $S_{Fp}$  is the spectral density of the fluctuating force  $F_p$  on the windward wall. The r.m.s. of the fluctuating force  $F_p$  is obtained by integration as follows

$$\sigma_{Fp} = \left[ \int_0^{n_c} \int_0^h \int_0^b \int_0^b \int_0^b \rho^2 C_p^2 U(z_1) U(z_2) S_u^{1/2}(z_1, n) S_u^{1/2}(z_2, n) \times \text{Coh}(y_1, y_2, z_1, z_2, n) dy_1 dy_2 dz_1 dz_2 dn \right]^{1/2} \quad (A5)$$

(Simiu and Scanlan 1996). This completes the calculation of the peak force  $F_{peak}$  induced by the ABL flow.

Step 2: Estimation of peak force  $F_{peak1}$  induced by the simplified flow.

The estimation process is similar to Step 1 except that:

1. The spectral density of the longitudinal velocity fluctuations  $u$  in the simplified flow is

$$S_u(z, n) = 0 \quad \text{for } 0 < f \leq f_{low}$$

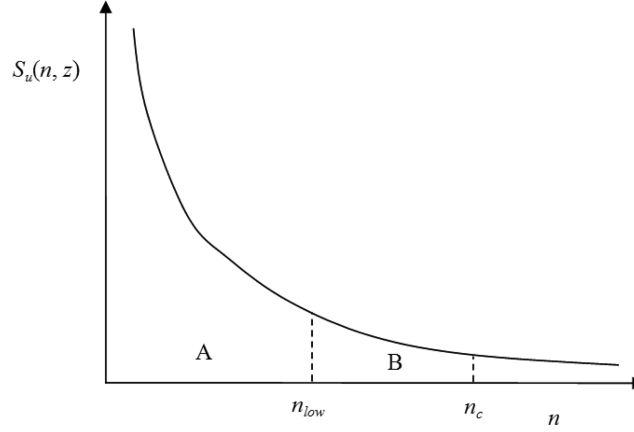


Fig. A1 Spectrum of the longitudinal velocity fluctuations [ $n = fU(z) / z$ ]

$$\frac{nS_u(z, n)}{u_*^2} = \frac{200f}{(1 + 50f)^{5/3}} \quad \text{for } f_{low} < f \leq f_c \quad (\text{A6})$$

where  $f_{low}$  can be selected near the lower limit of the interval within which the Kolmogorov inertial subrange hypothesis holds in the ABL wind, and  $f_c = 10$  as explained earlier. Recall that the reduced frequency  $f$  is based on mean wind speed  $U(z)$ .

The simplified flow has no (or weak) low-frequency fluctuations (area  $A$  in Fig. A1) (see Eq. A6), and has an increased mean speed  $cU$  which is required so that the peak force generated by the ABL flow (with speed  $U$  and spectral content denoted by  $A$  and  $B$  in Fig. A1) be the same as the peak force generated by the simplified flow (with speed  $cU$  and spectral content denoted by  $B$ ). Note that wind-induced pressures on buildings are affected by high-frequency fluctuations, which should be simulated in the simplified flow.

The calculation of the peak force  $F_{peak1}$  ( $= F_{cU}$ ) due to the simplified flow is similar to the calculation of the force  $F_{peak}$  in Step 1.

Step 3: Estimation of the upper limit of low-frequency fluctuations  $f_{low}$ .

To generate approximately equivalent peak forces due to the ABL flow (Step 1) and the simplified flow (Step 2), the low-frequency fluctuations must have sufficiently high spatial coherence so that the force they generate can be replaced by the mean force due to the incremental speed  $\Delta U$ . For small structures, e.g., residential homes, a reasonable approximate estimate of the upper limit of low-frequency fluctuations is  $f_{low} = 0.1$  (Yeo 2010).

Step 4, variant (a): Estimation of increased mean wind speed  $cU$ .

Given  $f_{low}$ , the increased mean wind speed  $cU = U + \Delta U$  can be determined by equating the peak force due to the ABL flow and the peak force due to the simplified flow (i.e.,  $F_{peak} = F_{peak1}$ ). The requisite factor  $c$  and the corresponding mean wind speed increment  $\Delta U$  are therefore estimated as follows

$$F_{cU} = c^2 F_U \quad (\text{A7})$$

$$c = \sqrt{\frac{\kappa_{Fp} \sigma_{Fp} - \kappa_{Fph} \sigma_{Fph}}{F_U} + 1} \quad (\text{A8})$$

$$\Delta U = (c - 1)U \quad (\text{A9})$$

where  $\kappa_{Fp}$  and  $\sigma_{Fp}$  are the peak factor and the r.m.s. of the fluctuating force, for all frequency fluctuations  $0 < f \leq f_c$ , and  $\kappa_{Fph}$  and  $\sigma_{Fph}$  are their counterparts corresponding to the high frequency fluctuations  $f_{low} < f \leq f_c$ .

Step 4, variant (b): Simplified estimation of increased mean wind speed  $c'U = U + \Delta U'$

An alternative estimate of the increased speed, denoted by  $c'U$  can be performed by equating the peak wind speed due to the low-frequency fluctuations in the ABL flow and the increment in the mean speed  $\Delta U'$  in the simplified flow. The results are then

$$U + \kappa_u \sigma_u = c'U + \kappa_{uh} \sigma_{uh} \quad (\text{A10})$$

$$c' = \frac{\kappa_u \sigma_u - \kappa_{uh} \sigma_{uh}}{U} + 1 \quad (\text{A11})$$

$$\Delta U' = \kappa_u \sigma_u - \kappa_{uh} \sigma_{uh} \quad (\text{A12})$$

where  $\kappa_u$  and  $\sigma_u$  are the peak factor and the r.m.s. of the longitudinally fluctuating wind speed corresponding to all frequency fluctuations  $0 < f \leq f_c$ , and  $\kappa_{uh}$  and  $\sigma_{uh}$  are their counterparts corresponding to high frequency  $f_{low} < f \leq f_c$ . The calculated  $\Delta U'$  is slightly more conservative (i.e., larger) and less accurate than  $\Delta U$  calculated in Step 4(a). The larger the building, the less accurate the simplified calculation is.

The software for the numerical implementation of the calculation is provided in Yeo (2010).