Application of waste tire rubber aggregate in porous concrete

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Abstract. This study aimed to categorize pervious rubberized concrete into fresh and hardened concrete analyzing its durability, permeability and strength. During the globalization of modern life, growing population and industry rate have signified a sustainable approach to all aspects of modern life. In recent years, pervious concrete (porous concrete) has significantly substituted for pavements due to its mechanical and environmental properties. On the other hand, scrap rubber tire has been also contributed with several disposal challenges. Considering the huge amount of annually tire wastes tossing out, the conditions become worse. Pervious concrete (PC) gap has graded surface assisted with storm water management, recharging groundwater sources and alleviate water run-offs. The results have shown that the use of waste tires as aggregate built into pervious concrete has tremendously reduced the scrap tire wastes enhancing environmental compliance.

Keywords: pervious concrete; rubber tire; waste; sustainability; environment

1. Introduction

Concrete is the single most widely used material in the world (Shariati 2008). It is an important construction material used extensively in buildings, bridges, roads and dams (Luo *et al.* 2019, Xie *et al.* 2019). Its uses range from

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structural applications, to paviors, kerbs, pipes and drains (Nosrati et al. 2018, Sajedi and Shariati 2019, Trung et al. 2019). Concrete as a composite material has different range of preparation depending on its application like its usage as high strength concrete (Arabnejad Khanouki et al. 2011, Shariati et al. 2011b, Shariati et al. 2012a, Shariati et al. et al. 2012d, 2012c, Shariati Shariati 2013. Mohammadhassani et al. 2014a, Mohammadhassani et al. 2014b, Mohammadhassani et al. 2014c, Shariati 2014, Shariati et al. 2014a, Shariati et al. 2014b, Khorramian et al. 2015, Shariati et al. 2015, Khanouki et al. 2016, Shahabi et al. 2016, Shariati et al. 2016, Khorramian et al. 2017, Nguyen-Sy et al. 2017, Hosseinpour et al. 2018, Nasrollahi et al. 2018, Ziaei-Nia et al. 2018) or light weight concrete (Shariati et al. 2010, Hamidian et al. 2011, Shariati et al. 2011a, Shariati et al. 2011c, Shariati et al. 2012b, Shariati et al. 2017, Vo-Duy et al. 2017, Ho-Huu et al. 2018, Davoodnabi et al. 2019) which are commonly used concrete in structures. Application of this important material in structure with special characteristics is extended to some other important usage in the life like pavement and roads. Pervious concrete (no-fines concrete) is one of them (Toghroli et al. 2017, Li et al. 2019, Bahari et al. 2018, Bahari et al. 2012).

It's a mixture of hydraulic cement, smaller coarse aggregates, admixtures and water, percolated by the concrete into subbase recharging the under-ground water levels (Sinaei *et al.* 2011, Ghosh *et al.* 2015). It is partly due

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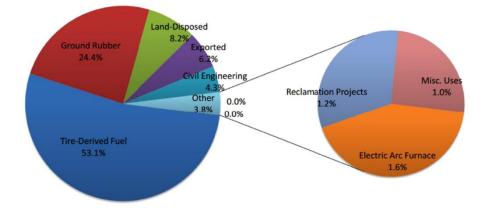


Fig. 1 Summary of US scrap market

to the impervious nature of the bituminous and concrete pavements. PC as an open-graded material has significant permeability due to the interconnected pores, ranging from 2 to 8 mm. Obtaining great amount of storm water seeping into the ground, PC has been taken in recharging groundwater and reducing storm water runoff (Talsania et al. 2015). Permeable concrete as PC has been applied to alleviate local flooding in urban eras providing water flowing in impermeable infrastructure (Kia et al. 2018). PC as porous concrete or enhanced porosity concrete is a macroporous concrete widely applied in sustainable constructions (Neithalath et al. 2010). Following the "zero-waste" notion, majority of US communities have focused on urban wastestreams and recycling industry. Accordingly, contribution of waste-stream materials with storm-water facilities like PC has significantly addressed the storm water treatment and the material's sustainability (Hager 2009). A research conducted by McGrath group has shown that approximately 40 million tons of recycled aggregates are manufactured in the UK every year which is only consisted of 20% of whole aggregates market (Ganjian et al. 2015). In order to achieve sustainable environment and development, waste management should be planned and developed meticulously prior to every construction project (Batayneh et al. 2007). Waste rubber tire has been globally considered hazardous gained by automobile industries. Regarding the non-biodegradability of waste rubber tires in nature, burning down the wastes is the cheapest decomposing solution, but resulting air pollution including greenhouse gases that signify the waste rubber tires' reapplication. Waste rubber is known for its noteworthy sustainability indicators such as embodied energy, material input factor, known as ecological rucksack, and carbon footprint. The value and the definition of these parameters are provided in Table 1. The reported values justify the necessity of reusing rubber instead of its disposal. Such justification is the main reason for current recycling rate of 300 million pounds of used rubber to crumb rubber annually. Because of the elasticity, lightweight, energy absorption, and heat insulating, it has been taken as a promising material in constructions (Ghosh et al. 2015).

The reliable performance of porous concrete as a structural component has been proved by various investigations. Also, steel-concrete composites were manufactured with lightweight and high strength concrete to evaluate the different loading and composition scenarios. Besides, applying lightweight concrete showed the outstanding results which satisfied the scholars to continue the use of this type of concrete in composite systems. Therefore, with respect to previous studies on the composite beams and floor systems, the pervious concrete could be a suitable replacement for lightweight concrete in these systems. Moreover, according to the properties of porous concrete, the hollow section thin-walled structures as steel rack systems could be reinforced with the lightweight pervious concrete (Shariati et al. 2010, Shariati et al. 2011c, Shariati et al. 2012b, Shariati et al. 2012a, Shariati et al. 2012f, Shariati et al. 2012e, Shariati 2013, Shariati et al. 2013, Shariati et al. 2014a, Shariati et al. 2014b, Khorramian et al. 2015, Shariati et al. 2015a, Khorramian et al. 2016, Shariati et al. 2016, Tahmasbi et al. 2016, Shariati et al. 2017b, Hosseinpour et al. 2018, Chen et al. 2019).

Hitherto various types of pervious concrete have been produced; hence, several experimental results are available which could be examined through the soft-computing, artificial intelligence algorithms, hybrid analytical solutions, or other analytical assessments. Therefore, the developed algorithms and the predicted results of pervious concrete are reliable sources for scholars or the construction industries (Sinaei et al. 2012, Toghroli et al. 2014, Khalilpasha et al. 2012, Sadeghi-Nik et al. 2012, Sadeghi-Nik et al. 2017 Hamdia et al. 2015, Mohammadhassani et al. 2015, Toghroli 2015, Mansouri et al. 2016, Safa et al. 2016, Thang et al. 2016, Toghroli et al. 2016, Khorami et al. 2017a, Tai et al. 2017, Sari et al. 2018, Sedghi et al. 2018, Toghroli et al. 2018a, Katebi et al. 2019, Mansouri et al. 2019, Shariati et al. 2019b, Shi et al. 2019b, Shariati et al. 2019a, Khorami et al. 2017b, Trung et al. 2019, Xu et al. 2019).

High-porosity is one of the major specifications of the pervious concrete. Since the thermal behavior of concrete depends on its porosity, it seems that the porous texture could be appealing to researchers who studied the thermal performance of concrete, especially at the elevated temperatures (Shahabi *et al.* 2016a, Davoodnabi *et al.* 2019).

Concerning the compressive strength range of pervious

Table 1 Sustainability indicators of rubber

Indicator	Definition	Value	Reference
Embodied Energy	The energy consumed by all of the processes associated with the production of a material from the extraction to manufacturing, transport and product delivery.	110 M Joules/kg	Kibert (2007)
Material Input Factor (Ecological Rucksack	the total mass (in kg) of m aterials removed from nature to produce a material	5 kg/kg	
Carbon Footprint	The mass of carbon dioxide released into the atmospher e due to the production of one unit mass of a matter	1.16-1.53 kgCO ₂ /kg matter	Sympath & Kennedy (2015)

concrete and its low tensile strength, using this kind of concrete is not a logical choice for cast in beams or steel tubes. However, applying the synthetic fibres or other additives could enhance the mechanical properties of pervious concrete to be used in the applications mentioned above (Arabnejad Khanouki *et al.* 2011, Shao *et al.* 2018, Sinaei *et al.* 2011, Shao *et al.* 2019, Mohammadhassani *et al.* 2014a, Mohammadhassani *et al.* 2014c, Arabnejad Khanouki *et al.* 2016a, Shah *et al.* 2016, Toghroli *et al.* 2017, Heydari and Shariati 2018, Luo *et al.* 2019, Wang *et al.* 2019, Xie *et al.* 2019, Shao and Vesel 2015, Shi *et al.* 2019a).

The word "pervious" typically refers to the porous concrete that is applied for pavement constructions. However, pervious concrete due to its high porosity and low density cannot perform like a high-performance or normal concrete. Thereby, the mechanical and chemical properties of pervious concrete could be improved not only for further studies but also for building industries (Arabnejad Khanouki *et al.* 2010, Abedini *et al.* 2017, Nosrati *et al.* 2018b, Abedini *et al.* 2019, Sajedi and Shariati 2019a). In addition, various methods are currently used to evaluate the structural health monitoring; hence, constructions produced from pervious concrete could be a proper option for the health monitoring process (Hamidian *et al.* 2012).

Also, the pervious concrete could be employed in steelconcrete composite structures due to the high mechanical strength. Since the dynamic behavior of the composite systems has always been of interest to researchers, constructions produced from pervious concrete could be investigated under seismic loading (Daie *et al.* 2011, Ghassemieh and Bahadori 2015, BAHADORI and Ghassemieh 2016).

According to Grubeša (2018), pervious permeable and no-fines concrete has carried similar literal components like the standard concrete, but with more porosity and void content (11% - 35%) and the water permeability coefficient of 2–6 mm/s. PC is the mix of cement, water, and coarse aggregate, with low fine aggregates. Due to the essentiality of pore connectivity in PC function, the related compaction is limited. In this study, the typical properties of PC have been highlighted like good drainage, high noise absorption, urban heat reduction, poor mechanical properties, low abrasion and freeze-thaw resistance (Grubeša *et al.* 2018, Peng *et al.* 2018). Waste tire rubber disposal globally would become an environmental problem (around 1000 million inefficient ones with 50% no further treatment), providing the waste tire-rubber usage in cement based substances replaced some of the natural aggregates (Thomas et al. 2016). On the other hand, the transportation cost of waste tires is averagely around £1/ton/km based on European Tire Recycling Association (ETRA) (Toghroli et al. 2018). PC pavements (PCPs) has provided run-off water to penetrate the ground to reduce the flash flooding risks produced by storm water run-off and also the water PCPs raising have reduced pollutant concentration in penetrating the captured water. Kfoury et al. (2015) determined that implementation of PCPs can prevent 700 million dollar losses due to halting service sectors during expected 4 days of rain precipitation at the city of Dubai. PC as a macro-porous concrete has excessively gained popularity due to its sustainable construction usage as parking lot, garages, and small roads in Europe (Switzerland and England). Initial favorable porous pavement usage has been performed for parking lots and service road in US (Kuo et al. 2013). Recycled PC aggregate as a new type of ecologically concrete has reduced the pollutions, protecting the ecological balance (Zhang et al. 2017). Permeable pavement is one of the propose techniques in Low Impact Developments (LID) in US and Water Sensitive Urban Design (WSUD) in Australia to minimize the urbanized impact by reducing the runoff peak flowing and making water quality control to save downstream waterbodies, largely through the following of natural processes (Razzaghmanesh and Beecham 2018). The performance of CPCs when exposed to sand and dust storm, a common environmental condition in arid regions, has been examined by El-Hassan et al. (2017). The results revealed that a properly designed PCP remains permeable despite of frequent sand accumulation and dust settlement on the pavement surface. In case of noticeable reduction in concrete permeability due to sand and dust pore clogging at top layer of pavement, cleaning with water jet could successfully recover the perviousness of pavement. Lower unit weights have been compared to plain concrete, less applicability of rubbrerized concrete with coarse rubber particles, significant decline in final strength and vivid elasticity modulus. More ductile behavior has been gained for rubberized concrete in comparison to plain concrete specimen(s) in compression testing (Khaloo et al. 2008).

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(a)

(b)

(c)

Fig. 2 (a) Waste tire, (b) Tire chip (TC) and (c) Crumb rubber (CR)

Total Municipal Solid Waste Generation in US has been illustrated (Fig. 1)(Thomas et al. 2016). Waste material usage by relatively replacement of cement in PC has reduced the cost of making concrete reducing the disposal problems of waste substances on cement usage for making PC. When cement has been substituted by different industrial wastes, compressive strength, flexural strength and split tensile strength and permeability of PC for different mixtures has depended on the waste materials' types used in PC making (TALSANIA et al. 2015). Usage of recycled aggregates from demolished concrete structures in PCPs was examined by Kianmehr et al. (2017). The results of compression and flexural tests revealed that the ratio of recycled aggregates should not exceed 30 percent of total aggregates. This limitation was mainly due to presence of weak aggregates and uncertainties associated with their adhesion to cementitious material in concrete mixture.

2. Categorizing waste rubber tyres

The rubber tires have been used by 3 various particlesize as very fine, fine and coarse including fine crumb rubber, crumb rubber (CR), tire chips (TC), replaced for cement and coarse aggregates. The concrete derived from rubber tire is named "rubberized concrete". Waste rubber tire, tire chip and CR are depicted in Figs. 2(a)-2(c) (Ghosh et al. 2015). Grinding and converting of tire rubber have been regarded as the most preferred method in tire recycling. CR concrete or asphalt pavement mixes have been sized (0.0075 mm - 4.75 mm), used in athletic tracks' outer surface, games, or its combinations such as asphalts (Thomas et al. 2016, Aoudia et al. 2017). (Gesoğlu et al. 2014b) has declared that the waste rubbers have been implemented in 3 diverse particle-size such as very fine, fine, and coarse, subsequently, TC in a gravity of 1.02 are applied as coarse rubber aggregate, while, 2 types of CR with nominal particle size (4 & 1 mm) are applied as fine aggregates in a 0.83 and 0.48 gravity. Despite technically viability, scrap tire usage in asphalt or other paving applications have been subsidized to compete the ordinary aggregate to meet the technical needs for asphalt pavement (Huang et al. 2007).

3. Properties of rubberized porous concrete

The rubber particles growing application as concrete aggregates has provoked the performance of rubberized PC in term of durability with low / limited strength resistance value (Shakrani et al. 2017). The mechanical properties of PC have indicated negative influence when waste rubber tires have been offered as its ingredients, say the rubber substances usage in PC has reduced its compressive strength and flexural strength, accordingly, despite of the compressive- strength reduction, it is in the approved range. Besides, the abrasion resistance and freeze thaw have been significantly improved; however, permeability is located within the confirmed curbs by using waste rubber tires, considered as fundamental required elements for PC pavement. So rubberized PC has been applied on less traffic roads, curbs, and shoulders (Ghosh et al. 2015). The strength reduction of rubberized concrete has brought prejudgments, however, the lower unit weight with higher sound and heat insulation, more resisting and roughness and raising flexibility features are the provisions juxtaposed with the ordinary concrete (Karakurt 2015).

3.1 Fresh concrete properties

3.1.1 Workability

(Eldin and Senouci 1993) have pioneered the research of aggregate obtained from the used tyres as the replacement of fine aggregate by the removed tyre rubber (size: 1 mm) and the replacement of coarse aggregate by discarded tyre rubber (size: 6, 19, 25 & 38 mm). The results have indicated the particular concrete with lower workability.

Mohammed *et al.* (2018) has studied the rubbercrete¹ made of partially replacement of fine aggregate in normal concrete with CR from scrap tires to optimize the mix ingredients turning out the rubbercrete to be more workable than the normal concrete (Mohammed *et al.* 2018). (Lv *et al.* 2015) has proved that the slump value of the fresh lightweight aggregate concrete has been declined by the raise of rubber-particles replacement because of the disorder shape and rough surface of rubber particles, respectively, the compressive-strength of RLAC² has

¹ Rubber-Concrete Composite

² Rubber Lightweight Aggregate Concrete

demonstrated a decline by raising the mixture ratio of the rubber particles content besides an increment with age. Furthermore, any minimizing in static modulus of elasticity has indicated great flexibility regarded as a favorable achievement in rubberized light-weight aggregate concrete mixes. In another study, (Thomas *et al.* 2016) has investigated the applicability of fresh concrete experimented in a compacting factor apparatus (IS 1199: 1959).

By growing percentages of concrete crumb rubber (CR), the density of the concrete has been declined because of the low specific gravity of CR compared to natural sand. Slump in fresh concrete mix has been reduced in high rubber waste mixture's contents. The drop in slump has depended on the amount and size of rubber particle in fresh concrete, respectively, in terms of size, the addition of rubber waste up to 10% has declined the slump (from 8.3 to 3.8 cm), and the addition of 20% rubber waste has decreased the slump (from 4.75 to 1.0 cm) (Toghroli *et al.* 2018). Also the study of (Benazzouk *et al.* 2006) has comprised the waste rubber particles of less than 1 mm (size) with approximate 20% polypropylene fibers. Consequently, total density of the rubber waste particle is 430 kg/m³.

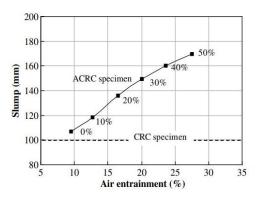


Fig. 3 Effect of air-entrainment on the slump of fresh composite containing different rubber volume ratios (0-50%)

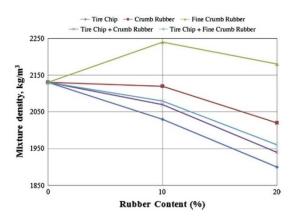


Fig. 4 Fresh density of PC versus rubber content

The composites derived from the application of the mentioned process have defined the cement rubber composite (CRC) and aerated cement rubber composite (ACRC). The applicability of fresh ACRC material has been significantly developed because of the generation of micro air bubbles on air-entraining agent addition. The influence of air-entrainment on the slump of a fresh aerated composite with changed rubber ratio has been offered (Fig. 3). (Li *et al.* 2004) has mentioned that 15% replacement of coarse aggregate through waste tire rubbers has reduced the influence of tire rubber wastes on the applicability of the changed concrete discarding chips / fiber.

3.1.2 Bulk density

By focusing on PC properties, (Gesoğlu et al. 2014b) has indicated that control PC has a density of 2130 kg/m³ (80% of normal concrete weight). Adding different rates of rubber has provided lighter concretes (Fig. 4) in a way that the rubberized PC densities are less than the control mixed one by 2-11%. The least density (1900 kg/m³) is gained from the mix of 20 TC, but the highest density (2240 kg/m^3) has belonged to the mix of 20 FCR, therefore, the rubberized concrete mixes are somehow applicable. Also the light weight concretes of air-entrainment in the fresh concrete have been increased by the minimized rubber particle size. Fresh concrete with rubber waste fraction 1/2 added to the 30 % of total aggregate (amount) has comprised the average air-entrainment of 5.3%, while samples with rubber waste fraction 0/1 have comprised air entrainment of 14.0% (Toghroli et al. 2018). Also, (Chandrappa and Biligiri 2016) have studied that adding of polymers and rubber have raised the fracture roughness of the material because of the ductility increment. The use of waste hardened concrete as a recycled aggregate on PC production has been investigated by Aliabdo et al. (2018). The effect of recycled concrete aggregate usage as a coarse aggregates replacement on fresh and hardened density has been depicted (Fig. 4), accordingly, using recycled concrete aggregates have relatively decreased the fresh and hardened density. Adding rubber particles in cement matrix has increased the air entrainment ratio, also the value range for CRC³ and ACRC⁴ specimen in 50% rubber volume level is (17.0% - 28.2%). For cement paste, air-entrainment has been changed (from 2.0% to 9.5%) in the same order (Benazzouk et al. 2006).

3.2 Hardened concrete characteristics

3.2.1 Compressive strength

The modification of PC properties by CR has indicated that the rubber adding has slightly decreased the strength and permeability, while significantly enhanced the ductility and freeze-thaw resistances (Liu *et al.* 2018), accordingly, the compressive-strength has been decreased by the raising of rubber incorporation range. Though the rubber addition has reduced the compressive strength of PC,

³ Cement-Rubber Composite

⁴ Arated Cement-Rubber Composite

the requirements of non-structural use have been met yet. (Khaloo et al. 2008) has observed more ductile behavior for rubberized concrete juxtaposed with the plain concrete specimen in compression testing. Another study conducted by Al-fadhl et al. (2017) has mentioned that the replacement of mineral aggregate by tire rubber particle in concrete has excessively reduced the final strength and tangential modulus of elasticity (Gesoğlu et al. 2014b). Mehmet et al. (2014) has investigated PC properties including waste tires proving that by using tire chips and CR, the compressive strength of porous concrete is 6.45 MPa, whereas, the compressive strength of PC is 3 to 30 MPa. However, CR has probably been used for the partially replacement of natural fine aggregate up to 7.5% with no adequate decline in its desired strength (Thomas et al. 2016). Meanwhile, (Biligiri and Mondal 2018) in their study have verified the hydrological, functional, and structural properties of 21 PC mixes encompassing 4 dosages of CR, 4 silica fume (SF) proportions, and 3 distinct aggregate gradation. Totally, 126 PC cylindrical tests have been performed to calculate density, porosity, permeability, abrasion resistance, and compressive strength, also their inclusion (CR & SF) in PC has made the compressive strength and abrasion resisting juxtaposed with the control original PC specimen. (Skripkiūnas et al. 2010) has also indicated that the compressive strength of rubberized concrete has depended on the rubber-waste's content and size which is reduced by more content and smaller size. (Xue and Shinozuka 2013) have declared the integration of cement paste and CR has been developed through the SF addition in concrete confirmed by the compressive-strength increment in rubberized SF concrete. (Ganjian et al. 2009) has investigated scrap tire rubber as a concrete aggregate, then the concrete mixtures' strength including chipped rubber has been decreased. Regarding the powder rubber replacement as 5%, the compressive-strength has been declined about 5% compared to the control mixture with 5% (weight) falling down in cement content. A replacement of 7.5% and 10% of powder rubber have decreased the strength about 10% to 23%, due to the cement reduction within the mixtures. (Warudkar and Valekar 2015) have investigated the concrete properties through the waste rubber as coarse aggregate, resulting that the compressive strength of rubberized concrete is low compared to normal concretes in the confirmed borders. The flexural strength has been decreased compared to normal concrete; however, the rubberish concrete cost is lower than normal concrete. High-strength rubber concrete has also been gained by magnesium oxychloride cement providing favourable bonding properties to rubber and essentially improving the rubbercrete performing. Furthermore, adhesion between rubber particles and other constituents substances have been surpassed by pre-treating the rubber aggregate with magnesium oxychloride (Siddique and Naik 2004). (Son et al. 2011) has studied the strength of PC by using waste rubber tire indicating that the compressive capacity of 24 MPa concrete has been decreased to 8 and 32% by 0.5 and 1% rubber particle addition to concrete mixture. Likewise, 0.5 and 1% rubber particle usage in the 28 MPa concrete mix has produced a 14% and 18% decline in the

compressive capacity of the column specimen. Another study has been conducted by (Mohammed and Adamu 2018) on roller-compacted rubbercrete by using the combined Son Reb and response surface methodology indicating that the compressive-strength, UPV⁵, RN⁶ and DMOE⁷ of RCR⁸ have been declined by the increase of replacement percentage of fine aggregate with CR⁹ above 10%. The addition of NS¹⁰ up to 2% has increased the compressivestrength, UPV, RN, and DMOE of RCR.

3.2.2 Flexural tensile strength

The flexural strength values from 2.16 to 0.40 MPa have indicated the highest strength value for control concrete (Fig. 5). Addition of rubber to PC has negatively influenced the flexural strength as in ordinary concrete providing a systematic decline by the rubber content's increment. When the rubber is substituted by natural aggregates, weak bonds between the cement paste and rubber particles have been formed compared to the stronger bonds between cement paste and aggregates. Therefore, based on the research, the rubber size is highly effectual on the flexural strength than the rubber content. PC with fine CR has provided the least flexural strength (Gesoğlu et al. 2014a). (Aliabdo et al. 2018) has defined the influence of recycled rubber aggregate's substitute ratio on the PC flexural strength. Based on the Fig. 5, any growing of substitute ratio of recycled aggregates has decreased the flexural strength of PC. The flexural strength reduction ratio because of recycled aggregate usage at 50%, 100% replacement level is 18.8% and 41.2%, therefore, on using 9.5 mm aggregate size, the flexural strength decreasing ratio is 34% and 54% to the 19 mm aggregate size usage, which is a behaviour similar to splitting tensile strength (Fig. 5). Adverse influence of the recycled aggregate's usage might be subjected to the weak properties of transition zone toward the recycled aggregates. Also, the transition zone has highly affected the concrete tensile strength.

3.2.3 Abrasion resistant

(Thomas *et al.* 2016) has studied the abrasion concrete resistance including waste rubber tire particles. The results have shown a favorable resisting of rubberized concrete in abrasion than the control mix. When the water cement range is 0.4, abrasion depth is 1.41 mm for control mixture and the abrasion depth for all mixtures up to 20%, the CR replacement is lower than 1.41 mm. (Kang *et al.* 2012) has also studied the abrasion resisting of rubberized concretes, so SF and CR are additives, in other words, SF has made the compressive strength and abrasion concrete resistances, so addition of CR has lessen the compressive strength, however, the abrasion concrete resistance has been inclined. SF concrete has provided a favourable abrasion resistance than control concrete, and the rubberized concrete has done

⁵ Ultrasonic Pulse Velocity

⁶ Rebound Number

⁷ Dynamic Modulus of Elasticity

⁸ Roller-compacted Rubbercrete

⁹ Crumb Rubber

¹⁰ Nano Silica

a satisfied abrasion resisting than SF concrete. (Pedro *et al.* 2018) has studied the durability performance of high performance concrete from the recycled aggregate, subsequently, 3 subsets of concrete with densified SF proportions of 0%, 5% and 10% (in addition to cement) have been taken. The results have shown that applied FRA¹¹ and CRA¹² have carried out the needs based on the European standards in terms of using recycled aggregate in concrete.

3.2.4 Water absorption, sorptivity and penetration

According to (Güneyisi et al. 2016), substituting the natural aggregate with recycled aggregate has resulted permeability coefficient raising, however, the mechanical properties of such concretes have been negatively affected up to a certain degree. (Liu et al. 2018) has shown the varieties of the permeability coefficient of PC vs rubber content (Fig. 6), thereafter, the addition of rubber has decreased the absorption for control mixture of 2.89%, so in a mixture with 10% CR is 3.15% and in a mix with 20% CR is 3.32%. The same pattern has been gained in the series with water cement ranges of 0.45 and 0.50. (Gesoğlu et al. 2014b) has observed that the permeability of PC has fallen down into 0.25 - 0.61 cm/s, recommending the pervious concrete limitations. (Aliabdo et al. 2018) has also indicated the effects of rubber fibers content on PC permeability (Fig. 7). According to the outcome, raising of rubber fibers content has increased the PC permeability, occurred because of the PC density reduction in the result of using rubber fibers as coarse aggregates. Comparing to control mix, an increase in PC permeability is 5.5% and 10.3% for 1.5% and 3% rubber fiber. (Gesoğlu et al. 2014b) has investigated about the mechanical characteristics and permeability, then three rubber types have been applied in producing the rubberized plain PC mixtures gained by some replacement of the rubber aggregate, furthermore, using of rubber has significantly aggravated the mechanical characteristics and PC permeability, but in various degrees based on the applied rubber's type and rate.

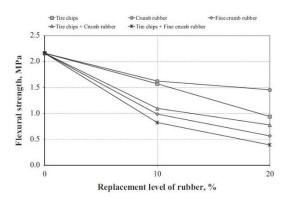


Fig. 5 Flexural strength of pervious concrete vs rubber replacement ratio

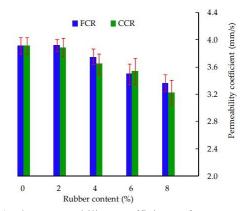


Fig. 6 The permeability coefficient of RMPC versus rubber content

3.2.5 Modules of elasticity

Typically, the replacement of rubber particle for aggregate and cement have reduced the modulus of concrete elasticity (Ganjian et al. 2009). (Gesoğlu et al. 2014b) has defined that the natural aggregate replacement by rubber particles has significantly increased the roughness and ductility of concrete beside the favorable damping capacity. The results have also indicated the incorporated PC with rubbers has a lower splitting tensile strength, modulus of elasticity, compressive strength of 3-30 MPa and permeability of 0.025-0.61 cm/s. In contrast, an obvious increment in the roughness, ductility and damping capacity of PC with rubbers have been observed. Application possibilities are in parking lots, crosses and road shoulders. The results of dynamic elasticity modulus of ACRC¹³ and CRC¹⁴ samples vs rubber particle content have been illustrated (Fig. 8) indicating a 50% rubber volume level. Besides, the dynamic features of elasticity on aerating a composite has been decreased about 6.2 to 3.7 GPa correspondent to 40.3% reduction. However, rubber has favoured the absorption of ultrasonic waves (Benazzouk et al. 2006). Accordingly, (Alaloul et al. 2018) has illustrated the results of the Modulus of Elasticity and Poisson's Ratio of concrete including CR. Any increasing in Nano silica ratio has increased the elasticity modulus and Poisson's ratio, because Nano silica is a pozzolanic material carrying the characteristics of a filler effect when reacted with portlandites matrix.

3.2.6 Freeze-thaw resistance

PC with macro-pore structure normally keeps water in the pores and might undergo F-T¹⁵ cycles deteriorating the material. F-T resistance has been calculated based on mass loss after a few successive freeze and thaw cycles. To determine the quantity of F-T resistance, various additives have been used (Toghroli *et al.* 2018). (Yang and Jiang 2003) have indicated that SF with super plasticizer has improved

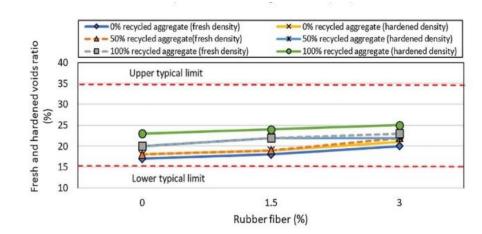
¹¹ Fine Recycled aggregates

¹² coarse recycled aggregates

¹³ Aerated Cement–Rubber Composite

¹⁴ Cement–Rubber Composite

¹⁵ Freeze-thaw



F-T resisting. Tire chips and CR are utilized to surpass the

affected the PC abrasion and freeze-thaw resistance.

Fig. 7 Effect of rubber fiber on PC voids ratio

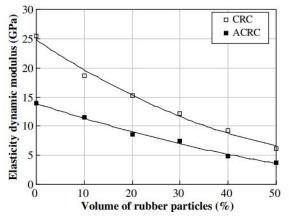


Fig. 8 Elasticity dynamic variations with rubber particles' volume ratio

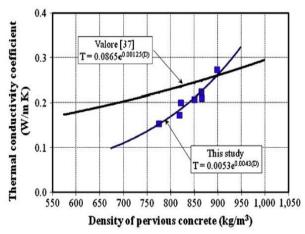


Fig. 9 The relations of density and thermal conductivity coefficient of LWCP

F-T resisting. Accordingly, the study on abrasion and freezing thawing resistance of PC by (Gesoğlu *et al.* 2014a) has shown that the rubber size and content have positively

Flexural strength reduction has been observed in rubber addition. The rubber usage after 300 freezing thawing cycles has been remarkably improved; also the rubber usage in various sizes and amounts has developed the surface property of PC through favourable abrasion resistance results in terms of wear-deep. (Toghroli et al. 2018) has declared that the frost resistance factor (Kf) has been applied in designing the composition of frost resistant concrete. in other words, adding rubber wastes have increased the closed porosity and frost resistant concrete provided no air-entraining agents through the control of cement parameters and rubberized-concrete. (Lund et al. 2018) has investigated the PC freeze thaw durability. In this research, the freeze-thaw durability of one PC baseline mix designed with 3 diverse entrained air levels have been evaluated through the use of operational modal analysis. Adding air entrainment has increased the PC applicability, so the void content has been reduced and the compressivestrength has been inclined. The effect of entrained air level in the cement paste on compressive-strength is not significant juxtaposed with the influence of void content.

3.2.7 Thermal and acoustic properties

(Khaloo *et al.* 2008) has investigated the feasibility of applying of elastic and flexible tire rubber aggregates in concrete, replaced as 12.5%, 25%, 37.5%, and 50% of total mineral aggregates in concrete. Tire–rubber concrete has potentially used in sound dampening and other shaking energies as sound insulation. (Chindaprasirt *et al.* 2015) has investigated the outcomes of thermal conductivity coefficient and weight reduction from abrasion test of light weight PC, then all light weight PC has lower thermal conductivity in 0.15 to 0.27 W/mK¹⁶ based on the content and type of additions because of the high porosity with less density of light weight aggregates and high void content of light weight PC. Also, (Chindaprasirt *et al.* 2015) has declared that the acoustic qualities of different materials would be verified based on the air flow resisting variations.

¹⁶ watts per meter-kelvin

The acoustic parameters of porous materials like foam gypsum slag, foam slag concrete and foam ceramic have been gained as frequency, porosity and the pores character. Porous and fibrous materials have been varied by porosity and macro-structure. (Licitra et al. 2019) has investigated the acoustic ageing of few rubberized road surfaces maintained based on the wet process laid on 3 various sites. Linear and logarithmic regression methods are used to say the acoustic ageing of the rubberized pavement. Rubberized asphalt pavement has been designed by an aggregate gradation finer with low susceptible to the acoustic ageing parameters. The analysis results of heat gain of a PCPC¹⁷ system compared to a PCC¹⁸ system have hypothesised that PC has behaved similarly to traditional concrete with similar material mix regarding the gain and loss of heat in summer days with less/no precipitation regardless of lower SRI¹⁹ in PC pavement (Haselbach et al. 2011). A study conducted by Park et al. (2015) has evaluated the physical and mechanical characteristics of sound absorption of porous concrete. Another study about the properties of sound absorption of the porous concrete by applying the recycled waste concrete aggregate has been conducted by (Park et al. 2005), resulting that the Noise Reduction Coefficient (NRC) is optimal at the void range of 25%, however, the percentage content of the recycled aggregates has low impact on NRC. Moreover, the optimal void range is 25% and the recycled aggregate is 50%. Acoustic qualities of different substances have been verified based on the air-flow resisting changes.

4. Conclusions

Using PC combined with scrap rubber tires as pavement is highly provisional in urban areas due to both intrinsic mechanical properties of porous concrete and environmental benefits of re-usage of waste rubber tires providing:

- Essential investigations on the properties of rubberized PC to meet the requirements of pavement porous concrete. In the following,
- Lack of compressive-strength and elasticity-modules of rubberized PC have also been observed.
- More ductile behaviors of the mentioned pavement concrete have led to lower bulk density and also lower tensile split.
- Consequently, using rubber in PC has reduced the permeability coefficient.
- On the other hand, the abrasion resistance has been improved when rubber is mixed in PC.
- Appropriate rubber size with additives has positively affected the rubberized PC mitigating the acoustic emissions.
- Rubberized PC has been taken as a highly promising material for pavements. Both mechanical and technical

properties have been fulfilled within the required standards in low-volume pavements as a considerable achievement in sustainable construction.

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¹⁷ Portland Cement Pervious Concrete

¹⁸ Portland Cement Concrete

¹⁹ Solar Reflectance Index

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Acronyms

SF= Silica fume (SF) PC= Pervious concrete (PC) PCPs= PC pavements (PCPs) CR= crumb rubber (CR) TC=tire chips (TC) UPV= Ultrasonic Pulse Velocity RN= Rebound Number DMOE= Dynamic Modulus of Elasticity RCR= Roller-compacted Rubbercrete CRC= Cement-Rubber Composite ACRC= Arated Cement-Rubber Composite F-T= Freeze Thaw