

Treatment of organic dye solutions by electrodialysis

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Abstract. Laboratory tests were performed to determine the efficiency of dye solution desalination by electrodialysis. The study involved anionic dye and mineral salt recovery by obtaining two streams from a salt and dye mixture – dye-rich solution and salt solution. A standard anion-exchange and cation-exchange membranes or monovalent selective anion-exchange membranes were used in the ED stack. It was found that the separation efficiency was strongly dependent on the dye molecular weight. The best results for standard ion-exchange membranes were achieved for the desalination of Direct Black solution. Furthermore, the obtained results implied that the application of monovalent selective anion-exchange membranes improved the recovery of dye and salt solutions – the dye concentration in the diluate remained constant irrespective of the molecular weight of anionic dyes, whereas the salt recovery remained very high (99.5%).

Keywords: dye; mineral salt; electrodialysis; monovalent selective anion-exchange membrane

1. Introduction

The textile industry produces huge amounts of waste waters heavily charged with unfixed dyes and other chemicals (salts, acids, hydroxides, dispersing and complexing agents, etc.). Purification of these complex effluents is therefore highly advisable, in view of the decrease of waste water volume, as well as the reuse of valuable substances. Among membrane processes, the electrodialysis seems to be very viable technology for the desalination of solutions containing organic substances.

Electrodialysis (ED) has been developed and applied for desalination and concentration of salty waters and industrial effluents since the 1950s (Baker 2000). Desalting of brackish waters and the production of boiler feed water and industrial process water are the main ED applications. And what is more, electrodialysis is one of the technologies that offer an opportunity to separate charged components from neutral substances. Fractionation of mono- and multi-valence ions of the same sign is also possible with the use of electro-membrane processes (Wang *et al.* 2012, Zhang *et al.* 2012).

Electrodialysis is now a technology which has been widely used in chemical, food and pharmaceutical industry (Tu 2005). The important ED applications involve: recovery of mineral and organic acids, milk whey desalination, desalination of protein products, glutamine and amino acids, production of vitamin C and lactic acid (Koter *et al.* 2011, Nagarale *et al.* 2006). On the other hand, there are only a few references dealing with direct application of electrodialysis in the

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treatment of salty industrial effluents. A waste water reclamation and reuse plant (Taiwan) established to treat effluents from steel production demonstrated the technical and economical feasibility of electrodialysis reversal (EDR) process (Chao and Liang 2008). A hybrid microfiltration (MF) and electrodialysis (ED) system was successfully employed to remove the color and contaminants of paper industry waste water (Nataraj *et al.* 2007). Chandramowleeswaran *et al.* (Chandramowleeswaran and Palanivelu 2006) proved that electrodialysis was also a promising technology for the treatment of textile effluents for TDS reduction to reuse the received water for production cycle.

Organic compounds are often very valuable fraction in waste waters. Some organic substances are non-charged and their separation from ionic constituents by ED seems to be rather easy. Singlande *et al.* (Singlande *et al.* 2006) found that acetic acid as a neutral compound was retaining in the course of ED process under the presence of mineral salt (NaCl and Na₂SO₄). The true difficulties arise when charged organics should be separated because they can migrate under the electric field conditions (Nataraj *et al.* 2007). Zhang *et al.* (2009) investigated separation of various organic compounds (acetate, glycine, aspartate, protonated lysine, methyl ammonium ion) in the ED process applying standard ion-exchange membranes and monoselective ion-exchange membranes. They concluded that the size effect took an important role in the separation of organic ions by ED.

The study aimed at the evaluation of the usability of electrodialysis process in the desalination of organic dye solutions. It was anticipated that by applying ion-exchange membranes and the electric field, separation of dye macroparticles from mineral salts will be possible. Although, organic dyes can dissociate in water solution, but taking into consideration the size of dye particles (1-10 nm), it does not seem probable that dyes will migrate through ion-exchange membranes.

The reported investigation is the continuation of the previous study (Majewska-Nowak 2010). The idea of the treatment of dye effluents from dye-house involves recovery of valuable substances (dyes, salts) and water reuse, and the integrated ultrafiltration-electrodialysis system was proposed (Fig. 1). Thus, the feed model solutions contain small dye amounts, characteristics of UF permeates.

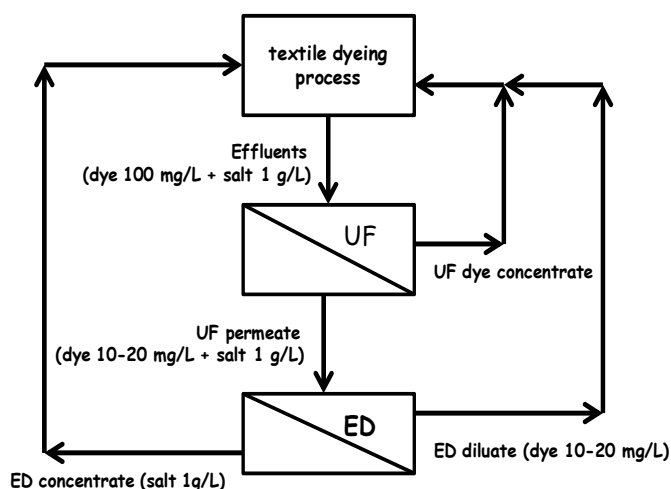


Fig. 1 The idea of dye effluent treatment by integrated UF-ED system

2. Materials and methods

2.1 Membranes and electrodialysis equipment

The study on the desalination of dye-salt mixtures was performed with use of a lab-scale electrodialysis apparatus. Standard PC-SK cation-exchange and PC-SA anion-exchange

Table 1 Properties of the ion-exchange membranes applied in the preliminary experiments

| Parameter | Membrane | |
|---|-------------------------------------|------------------------|
| | Cation-exchange (PC-SK) | Anion-exchange (PC-SA) |
| Producer | PCA GmbH (Germany) | |
| Thickness, μm | 90-130 | |
| Ion-exchange capacity, mmol/g | approx. 1.2 | approx. 1.1 |
| Electrical resistance, $\Omega\text{ cm}^2$ | 1 – 3 | 1 – 3 |
| Thermal stability, $^{\circ}\text{C}$ | Maximal 60 | Maximal 60 |
| Chemical stability (pH range) | 0 – 9 | 0 – 9 |
| Burst strength, MPa | 0.4 | 0.5 |
| Permselectivity (transfer number) | t- K^+ t- Cl^- | > 0.95 > 0.93 |
| Ionic form | Na^+ | Cl^- |
| Functional group | $-\text{SO}_3^-$ | $-\text{NR}_4^+$ |

Table 2 Properties of the ion-exchange membranes applied in the basic experiments

| Parameter | Membrane | |
|---|--|---|
| | Cation-exchange CMV Selemion ¹ | Anion-exchange ACS Neosepta ² |
| Producer | Asahi Glass Corp. (Japan) | Tokuyama Soda Corp. (Japan) |
| Thickness, μm | 130 – 150 | 150 – 200 |
| Ion-exchange capacity, mmol/g | approx. 2.4 | 1.4 – 2.0 |
| Electrical resistance, $\Omega\text{ cm}^2$ | 2.0 – 3.5 (0.5 M NaCl) | 2 – 2.5 (0.5 M NaCl) |
| Thermal stability, $^{\circ}\text{C}$ | Maximal 40 | High |
| Chemical stability | High | High |
| Burst strength, MPa | 0.16 | 0.15 |
| Permselectivity (transfer number) | t- Na^+ t- Cl^- | > 0.96 > 0.98 |
| Permselectivity (transfer number) of multivalence anions (SO_4^{2-}) | – | < 0.005 |
| Ionic form | Na^+ | Cl^- |
| Functional group | $-\text{SO}_3^-$ | $-\text{NR}_4^+$ |

¹ data available at <http://www.agec.co.jp>

² data available at <http://www.astom-corp.jp>

Table 3 Characteristics of two-chamber electro dialysis stack PCCell 64002

| | |
|--|--------------------------|
| Membrane size , cm | 11 × 11 |
| Effective membrane area, cm ² | 64 |
| Cell thickness, mm | 0.5 |
| Number of cell pairs | Up to 20 |
| Anode | Platinum coated titanium |
| Cathode | Steel V4A |
| Electrode housing | Polypropylene |

membranes (PCA GmbH, Germany) were used in the preliminary tests (Table 1). Standard CMV Selemion (Asahi Glass, Japan) cation-exchange and monovalent selective ACS Neosepta (Tokuyama Soda, Japan) anion-exchange membranes were chosen for basic experiments (Table 2). Each membrane had an effective area of 64 cm².

There were 10 cell pairs in the ED stack. Each cell pair contained a diluate and a concentrate compartment, thus 10 anion-exchange and 11 cation-exchange membranes were arranged in the stack (PCCell ED 64002 manual 2010). The ED stack operated as an integral part of the installation PCCell BED-1 produced by PCCell GmbH, Germany (Fig. 2, Table 3) (PCCell ED 64002 manual 2010).

2.2 Experimental and analytical methods

The electro dialysis desalination process was carried out for water salt solution and model salt solution containing various organic dyes (Merck, Zchem) (Table 4). The applied dyes were of an anionic type and varied in molecular weight. Dye concentration in the feed (diluate) solutions amounted to 8-12 mg/L. This range of concentration was characteristics of UF permeates after dye solution decolorization with the use of ceramic membranes (cut-off 5-30 kDa) (Majewska-Nowak 2010). Sodium chloride (NaCl) was used as a mineral salt in water solutions and dye aqueous mixtures. Salt concentration in the feed (diluate) water solutions was equal to 1, 2, 5, and 10 g NaCl/L, whereas for ED experiments with organic dyes, the dye mixtures containing 1 g NaCl/L were used.

In the course of ED experiments, the volume of diluate and concentrate was equal to 2 L. As initial concentrate and diluate, the same salt solution was used. However, the organic dyes were added only to diluate feed solutions. 0.1 N H₂SO₄ solution was used as an electrode rinsing solution.

The ED desalination experiments were performed at a constant electrical current and the applied current density was equal to 3.12, 6.24, 15.6, and 31.2 mA/cm² (salt water solutions) and to 1.56 mA/cm² (dye-salt mixtures). The determined limiting current density (for initial salt concentration equal to 1 g NaCl/L) was equal to 1.64 and 1.54 mA/cm² for ED process with standard PC-SA membranes and monovalent selective ACS membranes, respectively.

The ED system operated in a batch mode, i.e., both diluate and concentrate circulated (at the flow rate equal to 90 L/h) in the stack till the end of desalination process. The process was stopped when the maximum voltage had been achieved (24.5 V). Further continuation of the desalination brought the decrease in the applied current.

During the ED process diluate and concentrate samples were collected every 5-10 minutes. The variation in voltage was also monitored. The concentrations of organic dyes in both diluate

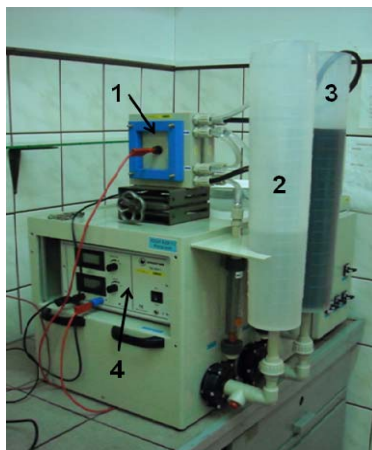


Fig. 2 Electrodialysis installation PCCell: 1 – electrodialysis stack, 2 – concentrate tank, 3 – diluate tank, 4 – power supply

Table 4 Characteristics of the experimental dyes

| Dye | Molecular weight, Da | Classification | pH ¹ | Dye symbol | λ_{\max} , ² nm | Structural formula |
|--|----------------------|----------------|-----------------|------------|------------------------------------|-----------------------------------|
| Methyl Orange C.I. ³ 13025 | 327 | Acid dye | 5.7 | MO | 465 | $C_{14}H_{14}N_9O_9SNa$ |
| Indigo Carmine C.I. 73015 | 466 | Acid dye | 5.5 | IC | 610 | $C_{16}H_8N_2Na_2O_8S_2$ |
| Amido Black C.I. 20470 | 615 | Acid dye | 5.7 | AB | 618 | $C_{22}H_{14}N_6Na_2O_9S_2$ |
| Titan Yellow C.I. 19540 | 696 | Direct dye | 5.5 | TY | 399 | $C_{28}H_{19}N_5Na_2O_6S_4$ |
| Direct Green C.I. 30315 | 878 | Direct dye | 6.1 | DG | 370 | $C_{35}H_{21}N_8Na_3O_{12}S_2$ |
| Direct Blue C.I. 34140 | 1029 | Direct dye | 7.2 | HB | 577 | $C_{40}H_{23}N_7Na_4O_{13}S_4$ |
| Direct Black C.I. 35435 | 1084 | Direct dye | 7.6 | DB | 585 | $C_{44}H_{32}N_{13}O_{11}S_3Na_3$ |

¹ Determined for the dye solutions of concentration equal to 100 mg/L

² Wavelength corresponding to the maximum absorbance of the dye solution

³ Colour Index number

and concentrate were determined spectrophotometrically at the wavelengths (λ_{\max}) given in Table 4, which correspond to the maximum absorbance of the sample. A spectrophotometer UVMINI-1240 (Shimadzu) and glass cuvettes with 1 cm optical lengths were used to determine dye solution absorbance. Analytical calibration curves of all dyes tested were found to be linear in the range of 1-10 mg/L.

Salt concentration in diluate and concentrate was determined indirectly by measuring the solution conductivity (with the use of conductivity meter Elmetron CC-411).

Electrical energy consumption (EC) in the ED desalination of dye-salt mixtures was calculated

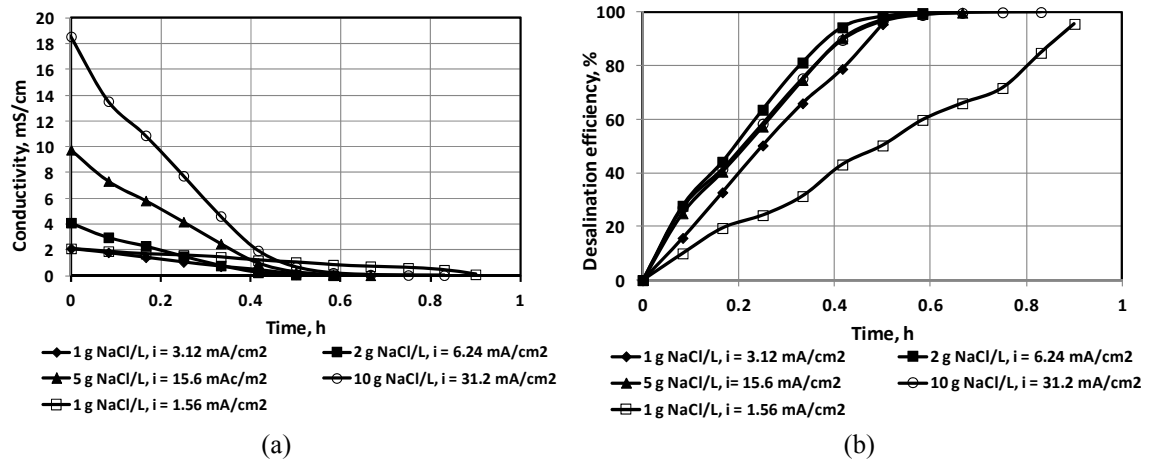


Fig. 3 Desalination of NaCl solutions by electrodialysis: (a) diluate conductivity versus operation time; (b) desalination efficiency versus operation time for various salt content

using the Eq.(1)

$$EC = \frac{I \int_0^t U dt}{V_d} \quad (1)$$

where

EC – electrical energy demand per 1 m³ of treated solution, kWh/m³

I – current intensity, A

U – voltage, V

V_d – volume of the diluate, m³

t – time of the process, s

3. Results and discussion

3.1 Preliminary tests on saline water desalination with the use of standard ion-exchange membranes

The aim of these preliminary tests was to evaluate the ED desalination process with the use of standard PCA membranes, as well as to verify the operation conditions of the PCCell BED-1 installation. The operational parameters, i.e., the applied electrical current have been chosen in such way to not exceed the limiting current density. The limiting current density was evaluated theoretically on the basis of Rautenbach et al. (Rautenbach and Albrecht 1989) approach with assumption that the final salt concentration in the diluate cells should not exceed 5-10% of the initial salt concentration.

The effect of salt content in the treated solution on ED efficiency is shown in the Fig. 3. The obtained desalination efficiency at a constant current density was rather high (90-95.5%), irrespectively of the initial salt concentration. However, the final diluate concentrations varied in a

great extend and amounted to 96; 239; 971 and 1949 $\mu\text{S}/\text{cm}$ for NaCl content equal to 1, 2, 5 and 10 g/L, respectively. It was also possible to reach very low diluate conductivity (in the range of 25–45 $\mu\text{S}/\text{cm}$) for all experiments, but this brought about the decrease in the current density. The results plotted in Fig. 3 involve also data for decreasing applied current, i.e., to reach maximal desalination degree.

It was also observed that the desalination time increases with the increasing salt content, although the applied current was increased proportionally, according to the Faraday's law. This finding can be attributed to the worsening of the conditions of the ion selective migration, due to the increased concentration gradient between concentrate and diluate cell.

3.2 Desalination of dye-salt mixtures with the use of standard ion-exchange membranes

First of all, the experiments aimed at evaluating the application of electrodialysis for desalination of dye-salt solutions. The most important was to receive two streams after ED process: dye solution free of mineral salt and salt solution free of dye particles. Moreover, the dye concentration in the diluate should remain constant at the level comparable to the initial dye concentration.

The effect of the dye molecular weight on the ED efficiency was verified. The experiments were carried out for six organic dyes of anionic type. The feed solutions contained dyes at concentrations typical of UF permeates, whereas NaCl concentration was equal to 1 g/L, both in diluate and concentrate feed solutions.

Fig. 4 gives the plots of dye concentrations in diluate and concentrate in the course of electrodialysis process with standard ion-exchange membranes. According to these plots, it can be concluded that only for one dye solution, i.e. containing Direct Black, the desalination result was

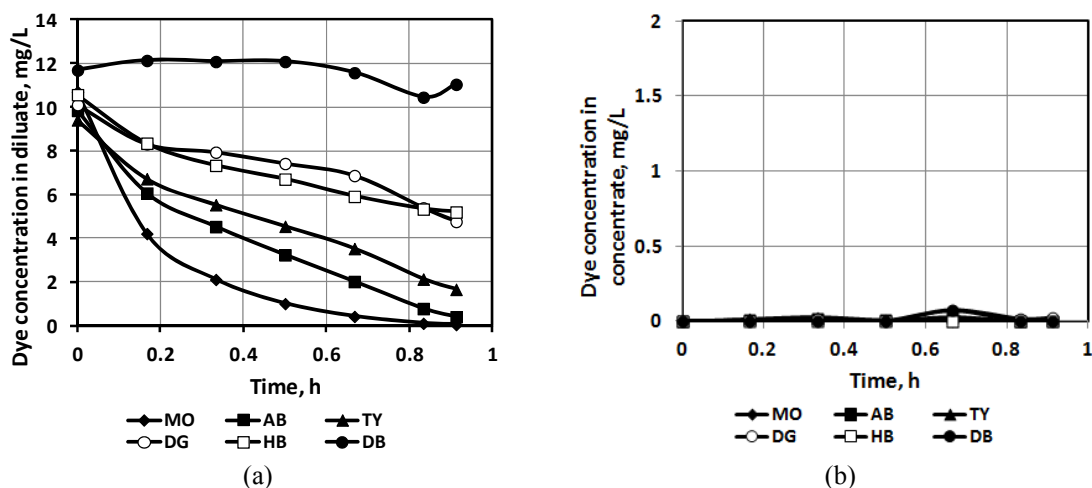


Fig. 4 Desalination of dye-salt mixtures with the use of standard ion-exchange membranes: (a) dye concentration in diluate versus time of ED process; (b) dye concentration in concentrate versus time of ED process for various organic anionic dyes. Current density – 1.56 mA/cm²; initial NaCl concentration in diluate and concentrate – 1 g NaCl/L

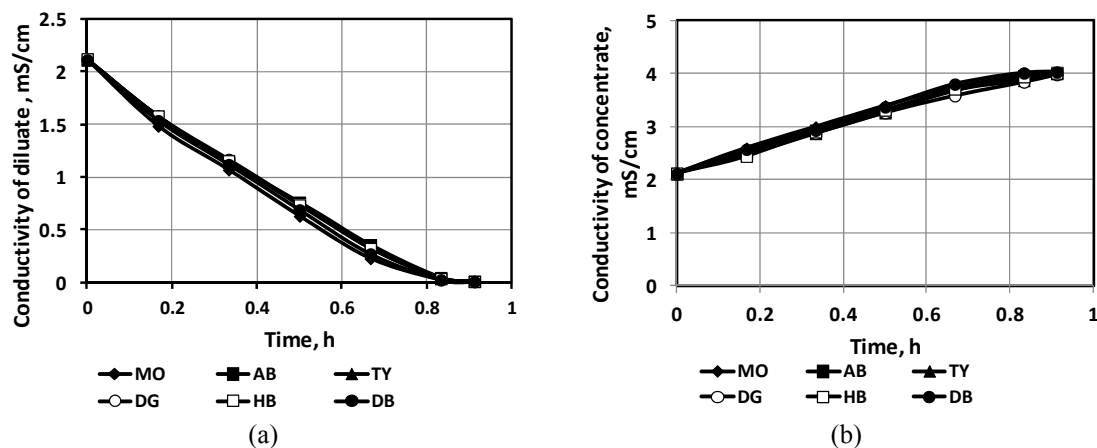


Fig. 5 Desalination of dye-salt mixtures with the use of standard ion-exchange membranes: (a) diluate conductivity versus time of ED process; (b) concentrate conductivity versus time of ED process for various organic anionic dyes. Current density – 1.56 mA/cm²; initial NaCl concentration in diluate and concentrate – 1 g NaCl/L

satisfactory – the dye concentration in the diluate was maintained at a nearly constant level, whereas almost complete salt removal was achieved. The other experimental dyes behaved in a quite different way – the dye concentration was decreasing with increasing operation time, although there was no migration of dye particles into concentrate cells. This phenomenon was more pronounced for dyes characterized by lower molecular weights. Such behavior of anionic dyes indicates that dye particles are subjected to membrane sorption phenomenon. The dye molecules adsorbed onto the membrane surface since the PC-SA membrane surface is positively charged. On the other hand, only when the highest-molecular-weight dye was tested, its penetration into anion-exchange membrane was impossible. It can be concluded that the size effect could also take a role (to some extent) in the separation of various organic dyes from mineral salt by electrodialysis with standard ion-exchange membranes. The importance of geometrical factors (the molecular size of organic substances and the network structure of membranes) was also mentioned by Tanaka *et al.* (2012) and Zhang *et al.* (2009).

3.3 Desalination of dye-salt mixtures with the use of standard cation-exchange membranes and monovalent selective anion-exchange membranes

Taking into consideration the main goal of the experiments, i.e. receiving of the two valuable streams (dye solution and salt solution) from a waste effluent, the further step of the study involved application of monovalent selective anion exchange membranes instead of a standard type. The use of standard ion-exchange membranes gave satisfactory results only in case of one dye – Direct Black (Fig. 4). It was anticipated that replacement of anion-exchange membranes by mono-anion-exchange membranes would hinder the migration of dye macro-anions into anion-exchange membranes.

The results of ED desalination of salt solutions containing various anionic dyes are shown in Figs. 6 and 7. The plotted relationships revealed that it was possible to keep the dye concentration

in the diluate at a constant value, irrespectively of the dye molecular weight. The implemented mono-selective anion-exchange membranes were a sufficient barrier to stop the migration of dye macro-anion into the membranes. In ED experiments with ACS membranes, the dye molecules were difficult to adsorb onto the membrane surface since monovalent selective anion-exchange membrane has negatively charged functional groups which repulse the dye molecules with the same charge sign. On the other hand, the transport of small mineral anions occurred with no obstruction. However, after 50 minutes of operation the electrical conductivity of the diluate received with ACS membranes was slightly higher than the electrical conductivity of the diluate obtained with PC-SA membranes (approximately $100 \mu\text{S}/\text{cm}$ and $40 \mu\text{S}/\text{cm}$, respectively) (Figs. 5 and 7). This can be explained by the fact that the electrical resistance of the ACS membranes is higher than the resistance of PC-SA membranes (Tables 1 and 2). Thus, the limiting voltage drop (24.5 V) was reached earlier when the ACS membranes were used.

The applied membrane combination enabled complete separation of dye particles from mineral salt.

The electrical energy consumption (EC) in the course of the electrodialysis of dye-salt solutions was calculated (Table 5). From the results obtained in can be inferred that the power consumption is almost of the same value for all tested solutions, including aqueous salt solution (with no dye addition). This finding is quite obvious in the view of Faraday's law. However, a slight shift towards higher power demand was observed with the increasing of dye molecular weight. This can be probably attributed to the hampered ion transport in the presence of large dye macro-anions and increasing cell resistance. Nevertheless, the calculated power consumption is very sensible. It should be noted that the data given in Table 4 do not involve energy demand for pumping of circulated solutions in the ED installation.

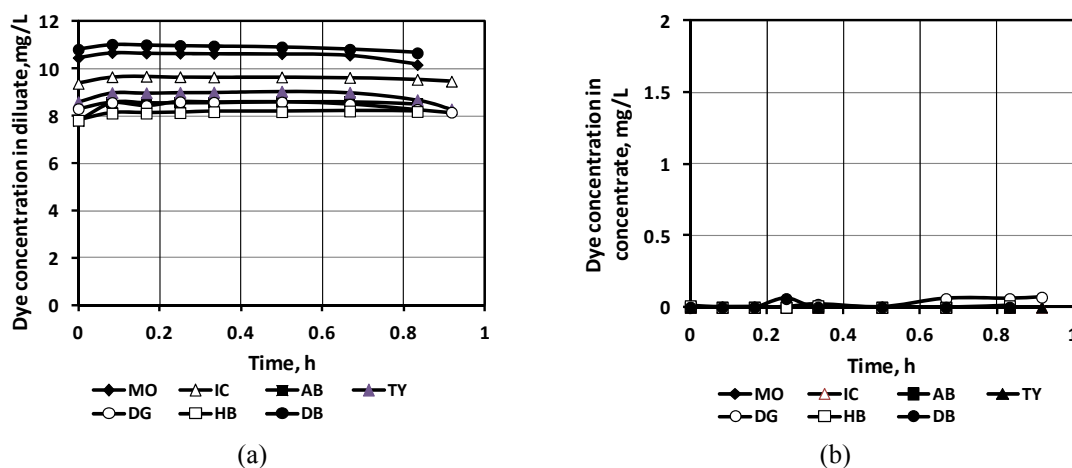


Fig. 6 Desalination of dye-salt mixtures with the use of standard cation-exchange membranes and monoselective anion-exchange membranes: (a) dye concentration in diluate versus time of ED process; (b) dye concentration in concentrate versus time of ED process for various organic anionic dyes. Current density – $1.56 \text{ mA}/\text{cm}^2$; initial NaCl concentration in diluate and concentrate – $1 \text{ g NaCl}/\text{L}$

Table 5 Energy consumption (EC) for ED desalination of dye-salt mixtures
(salt 1 g NaCl/L, $i = 1.56 \text{ mA/cm}^2$)

| Dye parameter | MO | IC | AB | TY | DG | HB | DB | H ₂ O |
|--------------------------|------|------|------|------|------|------|------|------------------|
| EC (kWh/m ³) | 0.38 | 0.40 | 0.49 | 0.55 | 0.48 | 0.48 | 0.49 | 0.47 |

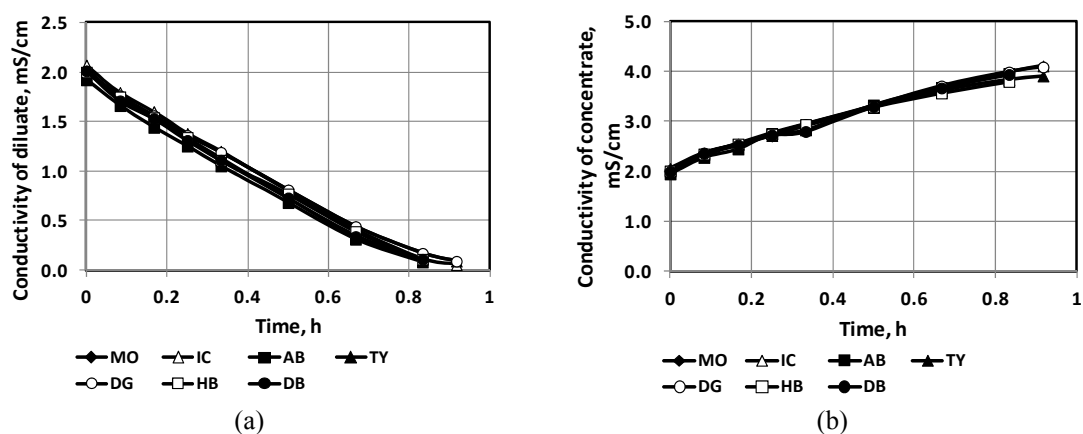


Fig. 7 Desalination of dye-salt mixtures with the use of of standard cation-exchange membranes and monoselective anion-exchange membranes: (a) diluate conductivity versus time of ED process; (b) concentrate conductivity versus time of ED process for various organic anionic dyes. Current density – 1.56 mA/cm^2 ; initial NaCl concentration in diluate and concentrate – 1 g NaCl/L

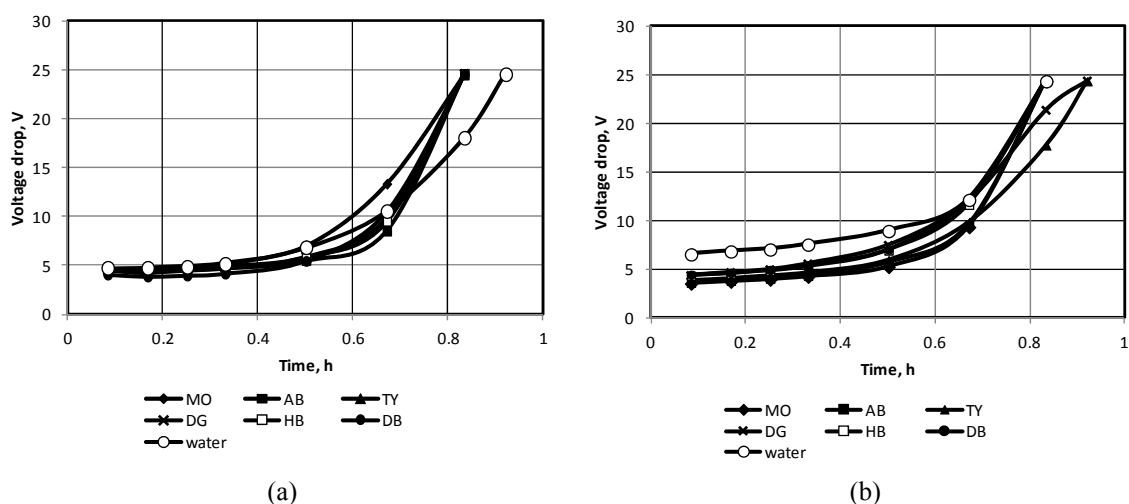


Fig. 8 Voltage drop in the ED stack during the experiments with standard anion-exchange membranes PC-SA (a); and monovalent selective anion-exchange membranes ACS (b). Current density – 1.56 mA/cm^2 ; initial NaCl concentration in diluate and concentrate – 1 g NaCl/L ; initial dye concentration in diluate – $8-10 \text{ mg/L}$

3.4 Voltage variation with time in the ED desalination of dye-salt mixtures

Organic fouling of anion-exchange membranes could be an important drawback of ED process during the desalination of various effluent streams (e.g., dye wastewaters). According to the results plotted in Figs. 5 and 7 it can be concluded that both membranes (i.e., standard anion-exchange PC-SA and monovalent selective anion-exchange ACS) were not fouled by the dye molecules. The extent of the fouling phenomenon can be also evaluated from the time-voltage curves. Fig. 8 shows the relationship between the voltage drop and operation time during the ED process with PC-SA membranes (Fig. 8(a)) and ACS membranes (Fig. 8(b)). The results have been plotted for dye-salt mixtures and for solutions containing only salt (1 g NaCl/L).

The results obtained confirmed the previous observations – the course of voltage drop for pure salt solutions and for dye-salt mixtures was similar, indicating the lack of fouling phenomenon in the first 40 minutes of ED operation. The insignificant fouling appeared in the case of experiments with PC-SA membranes (higher slopes of voltage-time curves for dye-salt solutions than slope for salt solution). It seems that monovalent selective anion-exchange membranes (ACS) exhibited much less susceptibility to fouling by dye molecules (Fig. 8(b)) than PC-SA membranes. It may be assumed that this inconsiderable fouling was observed due to rather low dye content in the treated solutions (8-12 mg/L).

4. Conclusions

1. The electrodialysis process with standard ion-exchange membranes enabled efficient desalination of organic dye solutions only for high-molecular-weight dye (Direct Black). The concentration of low-molecular-weight dyes in the diluate decreased with operation time, which was attributed to the sorption of dye particles in the membrane structure.
2. The size effect took an important role in the separation of various organic dyes from mineral salt by electrodialysis with standard ion-exchange membranes.
3. The electrodialysis with standard cation-exchange and monovalent selective anion-exchange membranes allowed satisfactory desalination of anionic dye solution, irrespectively of the dye type. Two streams from a salt and dye mixtures were received – one being enriched with dye alone (diluate), and the other one being a salt solution with no organic matter (concentrate).

Acknowledgements

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References

- Baker, R.W. (2000), *Membrane Technology and Application*, McGraw Hill, NJ, USA.
- Chandramowleeswaran, M., Palanivelu, K. (2006), "Treatability studies on textile effluent for total dissolved solids reduction using electrodialysis", *Desalination*, **201**(1-3), 164-174.
- Chao, Y.M. and Liang, T.M. (2008), "A feasibility study of industrial wastewater recovery using electrodialysis reversal", *Desalination*, **221**(1-3), 433-439.

- Koter S., Kultys, M. and Gilewicz-Lukasik, B. (2011) "Modeling the electric transport of HCl and H₃PO₄ mixture through anion-exchange membranes", *Membr. Water Treatment, Int. J.*, **2**(3), 187-205.
- Majewska-Nowak, K. (2010), "Application of ceramic membranes for the separation of dye particles", *Desalination*, **254**(1-3), 185-191.
- Nagarale, R.K., Gohil, G.S. and Shahi, V.K. (2006), "Recent developments on ion-exchange membranes and electro-membrane processes", *Adv. Colloid Interface Sci.*, **119**(2-3), 97-130.
- Nataraj, S.K., Sridhar, S., Shaikha, I.N., Reddy, D.S. and Aminabhavi, T.M. (2007), "Membrane-based microfiltration/electrodialysis hybrid process for the treatment of paper industry wastewater", *Sep. Purif. Technol.*, **57**(1), 185-192.
- PCCell ED 64002 manual (2010), "Operation and Maintenance Instruction", PCCell GmbH, Heusweiler, Germany, Version June 2010.
- Rautenbach, R. and Albrecht, R. (1989), *Membrane Processes*, John Wiley & Sons Ltd.
- Singlande, E., Balmann H.R., Lefevbre, X. and Sperandio, M. (2006), "Improvement of the treatment of salted liquid waste by integrated electrodialysis upstream biological treatment", *Desalination*, **199**(1-3), 64-67.
- Tanaka, N., Nagase, M. and Higa, M. (2012), "Organic fouling behaviour of commercially available hydrocarbon-based anion-exchange membranes by various organic-fouling substances", *Desalination*, **296**, 81-86.
- Tu, X. (2005), "Ion exchange membranes: State of their development and perspective", *J. Membr. Sci.*, **263**(1-2), 1-29.
- Wang, X., Nie, Y., Zhang, X., Zhang, S. and Li, J. (2012), "Recovery of ionic liquids from dilute aqueous solutions by electrodialysis", *Desalination*, **285**(1), 205-212.
- Zhang, Y., Van der Bruggen, B., Pinoy, L. and Meesschaert, B. (2009), "Separation of nutrient ions and organic compounds from salts in RO concentrates by standard and monovalent selective ion-exchange membranes used in electrodialysis", *J. Membr. Sci.*, **332**(1-2), 104-112.
- Zhang, Y., Paepen, S., Pinoy, L., Meesschaert, B. and Van der Bruggen, B. (2012), "Selectrodialysis: Fractionation of divalent ions from monovalent ions in a novel electrodialysis stack", *Sep. Purif. Technol.*, **88**, 191-201.