

# Fractional order thermoelastic wave assessment in a two-dimension medium with voids

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**Abstract.** In this article, the generalized thermoelastic theory with fractional derivative is presented to estimate the variation of temperature, the components of stress, the components of displacement and the changes in volume fraction field in two-dimensional porous media. Easily, the exact solutions in the Laplace domain are obtained. By using Laplace and Fourier transformations with the eigenvalues method, the physical quantities are obtained analytically. The numerical results for all the physical quantities considered are implemented and presented graphically. The results display that the present model with the fractional derivative is reduced to the Lord and Shulman (LS) and the classical dynamical coupled (CT) theories when the fractional parameter is equivalent to one and the delay time is equal to zero and respectively.

**Keywords:** fractional derivative; Laplace-Fourier transforms; porous medium; eigenvalues approach

## 1. Introduction

The elastic mediums with voids are basically a porous medium whose skeleton (matrix) is an elastic solid and the interstices are voids (small pores) containing nothing of energetic or physical significance. The theory of linear elastic mediums with voids is a generalization of the classical theory of elasticity. The classical theory of elasticity is not appropriate for the study of various types of geological and biological materials. The theory of linear elastic materials with voids deals with the distribution of small pores or voids in the elastic materials, where the volume of the void is included among the kinematics variables. The theory reduces to the classical theory in the limiting case for which the volume of void tending to zero. The problems of porous fluid-saturated mediums have been investigated for numerous years. To overcome the first shortcoming in the classical uncoupled thermoelastic theory, Biot (1956) established the coupled thermoelastic theory that it provides two phenomena are not consistent with the physical observations. By postulating a new law of heat conduction to replace the classical Fourier law, the generalized thermoelastic theory with one relaxation time has been established by Lord and Shulman (1967). Fractional computing has been used successfully to modify many existing physical process models. In the second half of the nineteenth century, it can be said that the whole theory of fractional derivatives and integrals has been determined. The generalization of the concepts of derivatives and integrals to a non-integer order has been the

subject of several methods and various alternative definitions of fractional derivatives have emerged. In the context of generalized thermoelastic theories, Youssef (2010), Youssef and Al-Lehaibi (2010) have presented the generalized fractional-order thermoelastic of low and high thermal conductivities. Based on a Taylor expansion of time-fractional order, Ezzat (2011, Ezzat and El Karamany (2011), Ezzat and El-Karamany (2011) have given other model for a fractional order generalized thermo-elasticity. A new model is presented by using the heat conduction law as Sherief *et al.* (2010). As an important branch of mechanical properties of solid, the literature Abbas and Alzahrani (2016), Abbas and Kumar (2016, Abd-Elaziz *et al.* (2019), Alzahrani and Abbas (2016, Deswal and Kalkal (2014), Ezzat and El-Bary (2017), Hussein (2015), Kakar and Kakar (2014), Lata and Kaur (2019), Othman *et al.* (2013, Othman and Abd-Elaziz (2019, Sarkar and Lahiri (2013, Sur and Kanoria (2014, Wang *et al.* (2015), Youssef (2012) have considered different problems by numerical and analytical methods. Singh Singh (2007) studied the wave propagation in material with voids under the generalized thermoelastic theory. Marin (2009), Marin *et al.* (2017), Marin and Nicaise (2016), Marin *et al.* (2019) have presented some problems to study the elastic dipolar bodies. Karageorghis *et al.* (2014) have investigated the moving pseudo-boundary MFS in two-dimension thermoelastic materials with voids. Many authors Abbas (2007), Abbas (2009), Abbas (2014), Abbas (2014), Abbas *et al.* (2009, Hobiny and Abbas (2018), Kaur and Lata (2020, Lata and Kaur (2019), Lata and Zakhmi (2019), Mohamed *et al.* (2009) have presented the solutions of several problems under generalized thermo-elastic models. Ezzat *et al.* (2016) presented a modeling in generalized thermoelastic theory based on memory-dependent derivative. Sarkar (2017) used

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the time-fractional order two-temperature model to study the wave propagation in an initially stressed elastic half-space solids under magneto-thermoelastic theory. Ellahi *et al.* (2019), Sheikholeslami *et al.* (2019) have present the solutions for various porous medium problems under several boundary conditions. By using the fractional calculus, several actual models of physical procedures have been improved successfully. It can be safely said that all integrations models and fractional derivatives were formed in the last four decades. Otherwise, various methods and definitions of fractional derivatives have become the main object of several studies. In the domain of Laplace, the eigenvalue approaches gave the analytical solutions without any supposed restriction on the factual physical quantities.

The aim of this paper is to study the effects of fractional order derivative in a two-dimension porous medium. By using the Fourier-Laplace transforms and eigenvalues method based on an numerical and analytical methods, the governing equations are processed. For the considered physical quantities, the numerical outcomes are obtained and presented graphically.

## 2. Mathematical model

For an isotropic, elastic and homogeneous two-dimensional medium contains voids, the governing relations under generalized thermoelastic theory Lord and Shulman (1967), based on Cattaneo (1958) and Ezzat *et al.* (2014) and according to Singh (2007) in the absence of body forces and the heat source can be introduced by:

$$(\lambda + \mu)u_{j,i,j} + \mu u_{i,j,j} + b\varphi_{,i} - \gamma_t \Theta_{,i} = \rho \frac{\partial^2 u_i}{\partial t^2}, \quad (1)$$

$$(\lambda + \mu)u_{j,i,j} + \mu u_{i,j,j} + b\varphi_{,i} - \gamma_t \Theta_{,i} = \rho \frac{\partial^2 u_i}{\partial t^2}, \quad (2)$$

$$K\Theta_{,jj} = \left(1 + \frac{\tau_o^\beta}{\Gamma(\beta+1)} \frac{\partial^\beta}{\partial t^\beta}\right) \left(\rho c_e \frac{\partial \Theta}{\partial t} + mT_o \frac{\partial \varphi}{\partial t} + \gamma_t T_o \frac{\partial u_{j,j}}{\partial t}\right), \quad (3)$$

$0 < \beta \leq 1$

The stress-displacement equations can be given by

$$\sigma_{ij} = \mu(u_{i,j} + u_{j,i}) + (\lambda u_{k,k} + b\varphi - \gamma_t \Theta)\delta_{ij} \quad (4)$$

By taking into consideration the above definition can be expressed by

$$\frac{\partial^\beta g(\mathbf{r}, t)}{\partial t^\beta} = \begin{cases} g(\mathbf{r}, t) - g(\mathbf{r}, 0), & \beta \rightarrow 0, \\ I^{\alpha-1} \frac{\partial g(\mathbf{r}, t)}{\partial t}, & 0 < \beta < 1, \\ \frac{\partial g(\mathbf{r}, t)}{\partial t}, & \beta = 1, \end{cases} \quad (5)$$

where  $I^\beta$  is the Riemann-Liouville integral fraction introduced as a natural generalization of the well-known integral  $I^\beta g(\mathbf{r}, t)$  that can be written as a convolution type.

$$I^\beta g(\mathbf{r}, t) = \int_0^t \frac{(t-s)^\beta}{\Gamma(\beta)} g(\mathbf{r}, s) ds, \beta > 0 \quad (6)$$

where  $g(\mathbf{r}, t)$  is a Lebesgue's integral function and  $\Gamma(\beta)$  is the Gamma function. In the case where  $g(\mathbf{r}, t)$  is

definitely continuous, then it is possible to write

$$\lim_{\beta \rightarrow 1} \frac{\partial^\beta g(\mathbf{r}, t)}{\partial t^\beta} = \frac{\partial g(\mathbf{r}, t)}{\partial t} \quad (7)$$

This model can be reduced to:

i) (CT) point to the classical coupled model  $\tau_o = \beta = 0$ .

ii) (LS) point to Lord and Shulman's model  $\tau_o > 0, \beta = 1$ , where the different values of fractional parameter  $0 < \beta \leq 1$  cover two types of conductivity,  $\beta = 1$  for normal conductivity and  $0 < \beta < 1$  for low conductivity,  $\omega_o, \alpha, b, m, \psi, \zeta_1$  are the material constants due to presence of voids  $\tau_o$  is the thermal relaxation time,  $\sigma_{ij}$  are the components of stress,  $\rho$  is the density of material,  $\Theta = T - T_o$ ,  $T_o$  is the reference temperature,  $u_i$  are the components of displacement,  $K$  is the coefficient of thermal conductivity,  $\lambda, \mu$  are the Lamé's constants,  $c_e$  is the specific heat at constant strain,  $\gamma_t = (3\lambda + 2\mu)\alpha_t$ ,  $\alpha_t$  is the linear thermal expansion coefficient,  $t$  is the time and  $i, j, k = 1, 2, 3$ . We consider plane waves in the  $xy$ -plane therefore in the two-dimensional porous medium, we have

$$\mathbf{u} = (u, v, 0), u = u(x, y, t), v = v(x, y, t), \Theta = \Theta(x, y, t), \quad (8)$$

$$\varphi = \varphi(x, y, t).$$

Subsequently, the Eqs. (1)-(4) can be given by:

$$\rho \frac{\partial^2 u}{\partial t^2} = (\lambda + 2\mu) \frac{\partial^2 u}{\partial x^2} + (\lambda + \mu) \frac{\partial^2 v}{\partial x \partial y} + \mu \frac{\partial^2 u}{\partial y^2} + b \frac{\partial \varphi}{\partial x} - \gamma_t \frac{\partial \Theta}{\partial x} \quad (9)$$

$$\rho \frac{\partial^2 v}{\partial t^2} = (\lambda + 2\mu) \frac{\partial^2 v}{\partial y^2} + (\lambda + \mu) \frac{\partial^2 u}{\partial x \partial y} + \mu \frac{\partial^2 v}{\partial x^2} + b \frac{\partial \varphi}{\partial y} - \gamma_t \frac{\partial \Theta}{\partial y} \quad (10)$$

$$\rho \psi \frac{\partial^2 \varphi}{\partial t^2} = \alpha \left( \frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial y^2} \right) - \omega_o \frac{\partial \varphi}{\partial t} - \zeta_1 \varphi - b \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + m\Theta \quad (11)$$

$$K \left( \frac{\partial^2 \Theta}{\partial x^2} + \frac{\partial^2 \Theta}{\partial y^2} \right) = \left( 1 + \frac{\tau_o^\beta}{\Gamma(\beta+1)} \frac{\partial^\beta}{\partial t^\beta} \right) \left( \rho c_e \frac{\partial \Theta}{\partial t} + mT_o \frac{\partial \varphi}{\partial t} + \gamma_t T_o \frac{\partial}{\partial t} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) \right) \quad (12)$$

$$\sigma_{xx} = \lambda \frac{\partial v}{\partial y} + (\lambda + 2\mu) \frac{\partial u}{\partial x} + b\varphi - \gamma_t \Theta, \sigma_{xy} = \mu \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) \quad (13)$$

## 3. Application

The problem initial conditions can be taken by

$$\begin{aligned} \Theta(x, y, 0) = \frac{\partial \Theta(x, y, 0)}{\partial t} = 0, \varphi(x, y, 0) = \frac{\partial \varphi(x, y, 0)}{\partial t} = 0, u(x, y, 0) \\ = \frac{\partial u(x, y, 0)}{\partial t} = 0, v(x, y, 0) = \frac{\partial v(x, y, 0)}{\partial t} = 0. \end{aligned} \quad (14)$$

While, the appropriate boundary conditions can be expressed as

$$\begin{aligned} \sigma_{xx}(0, y, t) = \sigma_{xy}(0, y, t) = 0.0, -K \frac{\partial \Theta(0, y, t)}{\partial x} \\ = q_o \frac{t^2 e^{-\frac{t}{\tau_p}}}{16t_p^2} H(a - |y|), \frac{\partial \varphi(0, y, t)}{\partial x} = 0 \end{aligned} \quad (15)$$

where  $q_0$  is a constant  $H$  is the unit Heaviside function and  $t_p$  is the pulse heat flux characteristic time. For appropriateness, the dimensionless physical quantities can be defined by

$$\begin{aligned}\theta' &= \frac{\theta}{T_0}, (\sigma'_{xx}, \sigma'_{xy}) = \frac{(\sigma_{xx}, \sigma_{xy})}{(\lambda + 2\mu)}, (t', \tau'_0) \\ &= \eta c^2(t, \tau_0), (x', y', u', v') \\ &= \eta c(x, y, u, v), \varphi' = \psi \eta^2 c^2 \varphi\end{aligned}\quad (16)$$

where  $\eta = \frac{\rho c_e}{k}$  and  $c = \sqrt{\frac{\lambda + 2\mu}{\rho}}$ .

In these dimensionless parameters terms of the in Eq. (16), the above Eqs. (9)-(15) can be given by (the dashes have been neglected for convenience)

$$\frac{\partial^2 u}{\partial t^2} = \frac{\partial^2 u}{\partial x^2} + (1 - s_1) \frac{\partial^2 v}{\partial x \partial y} + s_1 \frac{\partial^2 u}{\partial y^2} + s_2 \frac{\partial \varphi}{\partial x} - s_3 \frac{\partial \theta}{\partial x} \quad (17)$$

$$\frac{\partial^2 v}{\partial t^2} = \frac{\partial^2 v}{\partial y^2} + (1 - s_1) \frac{\partial^2 u}{\partial x \partial y} + s_1 \frac{\partial^2 v}{\partial x^2} + s_2 \frac{\partial \varphi}{\partial y} - s_3 \frac{\partial \theta}{\partial y} \quad (18)$$

$$s_4 \frac{\partial^2 \varphi}{\partial t^2} = \frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial y^2} - s_5 \frac{\partial \varphi}{\partial t} - s_6 \varphi - s_7 \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + s_8 \theta \quad (19)$$

$$\frac{\partial^2 \theta}{\partial x^2} + \frac{\partial^2 \theta}{\partial y^2} = \left( 1 + \frac{\tau_0^\beta}{\Gamma(\beta + 1)} \frac{\partial^\beta}{\partial t^\beta} \right) \left( \frac{\partial \theta}{\partial t} + s_9 \frac{\partial \varphi}{\partial t} + s_{10} \frac{\partial}{\partial t} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) \right) \quad (20)$$

$$\sigma_{xx} = (1 - 2s_1) \frac{\partial v}{\partial y} + \frac{\partial u}{\partial x} + s_2 \varphi - s_3 \theta, \sigma_{xy} = s_1 \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) \quad (21)$$

$$\begin{aligned}\sigma_{xx}(0, y, t) &= \sigma_{xy}(0, y, t) = 0, \frac{\partial \theta(0, y, t)}{\partial x} \\ &= -q_0 \frac{t^2 e^{-\frac{t}{t_p}}}{16t_p^2} H(a - |y|), \frac{\partial \varphi(0, y, t)}{\partial x} = 0\end{aligned}\quad (22)$$

where

$$\begin{aligned}s_1 &= \frac{\mu}{\rho c^2}, \quad s_2 = \frac{b}{\rho \psi \eta^2 c^4}, \quad s_3 = \frac{\gamma_t T_0}{\rho c^2}, s_4 = \frac{\rho c^2 \psi}{a}, s_5 = \frac{\omega_0}{a \eta}, \\ s_6 &= \frac{\zeta_1}{a \eta^2 c^2}, s_7 = \frac{b \psi}{a}, s_8 = \frac{m \psi T_0}{a}, s_9 = \frac{m}{\psi \eta^3 c^2 k}, s_{10} = \frac{\gamma_t}{\rho c_e}.\end{aligned}$$

Now, the Laplace transforms for any function  $M(x, y, t)$ , are expressed as in Debnath and Bhatta (2014)

$$\bar{M}(x, y, s) = \int_0^\infty M(x, y, t) e^{-st} dt, s > 0, \quad (23)$$

while, the Fourier transforms for any function  $\bar{M}(x, y, s)$  are given as

$$\bar{M}^*(x, q, s) = \int_{-\infty}^\infty \bar{M}(x, y, s) e^{-iqy} dy. \quad (24)$$

Thus, the governing equations under initial conditions and using the boundary conditions are given to get the system of ordinary differential equations by

$$\frac{d^2 \bar{u}^*}{dx^2} = (s^2 + s_1 q^2) \bar{u}^* - iq(1 - s_1) \frac{d\bar{v}^*}{dx} - s_2 \frac{d\bar{\varphi}^*}{dx} + s_3 \frac{d\bar{\theta}^*}{dx} \quad (25)$$

$$\frac{d^2 \bar{v}^*}{dx^2} = \frac{(s^2 + q^2)}{s_1} \bar{v}^* - \frac{s_2 iq}{s_1} \bar{\varphi}^* + \frac{s_3 iq}{s_1} \bar{\theta}^* - \frac{iq(1 - s_1)}{s_1} \frac{d\bar{u}^*}{dx}, \quad (26)$$

$$\frac{d^2 \bar{\varphi}^*}{dx^2} = s_7 iq \bar{v}^* + (s^2 s_4 + q^2 + s_6 + s_5 s) \bar{\varphi}^* - s_8 \bar{\theta}^* + s_7 \frac{d\bar{u}^*}{dx} \quad (27)$$

$$\frac{d^2 \bar{\theta}^*}{dx^2} = s_{10} iq s \gamma \bar{v}^* + s_9 s \gamma \bar{\varphi}^* + (q^2 + s \gamma) \bar{\theta}^* + s \gamma s_{10} \frac{d\bar{u}^*}{dx} \quad (28)$$

$$\bar{\sigma}_{xx}^* = iq(1 - 2s_1) \bar{v}^* + \frac{d\bar{u}^*}{dx} + s_2 \bar{\varphi}^* - s_3 \bar{\theta}^* \quad (29)$$

$$\bar{\sigma}_{xy}^* = s_1 \left( \frac{d\bar{v}^*}{dx} + iq \bar{u}^* \right), \quad (30)$$

$$\bar{\sigma}_{xx}^* = \bar{\sigma}_{xy}^* = 0, \frac{d\bar{\varphi}^*}{dx} = 0, \frac{d\bar{\theta}^*}{dx} = -\frac{q_0 t_p}{8(st_p + 1)^3} \sqrt{\frac{2 \sin(qa)}{\pi q}} \quad (31)$$

where  $\gamma = 1 + \frac{s^\beta \tau_0^\beta}{\Gamma(\beta + 1)}$ . The differential equations vector-matrix of Eqs. (25-28) can be written by

$$\frac{dN}{dx} = AN \quad (32)$$

where  $N = [\bar{u}^* \quad \bar{v}^* \quad \bar{\varphi}^* \quad \bar{\theta}^* \quad \frac{d\bar{u}^*}{dx} \quad \frac{d\bar{v}^*}{dx} \quad \frac{d\bar{\varphi}^*}{dx} \quad \frac{d\bar{\theta}^*}{dx}]^T$  and the matrix  $A = [a_{ij}] = 0, i, j = 1 \dots 8$ .

Excepting  $a_{15} = a_{26} = a_{37} = a_{48} = 1$ ,

$$a_{51} = s^2 + s_1 q^2, a_{56} = -iq(1 - s_1), a_{57} = -s_2, a_{58} = s_3, a_{62} = \frac{(s^2 + q^2)}{s_1}, a_{63} = -\frac{s_2 iq}{s_1},$$

$$a_{64} = \frac{s_3 iq}{s_1}, a_{65} = -\frac{iq(1 - s_1)}{s_1}, a_{72} = s_7 iq, a_{73} = s^2 s_4 + q^2 + s_6 + s_5 s, a_{74} = -s_8, a_{75} = s_7,$$

$$a_{82} = s_{10} iq s \gamma, a_{83} = s_9 s \gamma, a_{84} = q^2 + s \gamma, a_{85} = s \gamma s_{10}.$$

By using the eigenvalues approach which proposition by Abbas (2015), Abbas *et al.* (2019), Das *et al.* (1997), the analytical solutions of Eq. (32) can be given. thereafter, the matrix  $A$  has the characteristic equation can be written as:

$$\xi^8 - f_4 \xi^6 + f_3 \xi^4 + f_2 \xi^2 + f_1 = 0 \quad (33)$$

where  $f_1, f_2, f_3$  and  $f_4$  can be defined as in appendix A. To get the solutions of Eq. (29), the eigenvalue and its eigenvector of matrix  $A$  should be calculated. In the cases  $\pm \xi_1, \pm \xi_2, \pm \xi_3, \pm \xi_4$  are the eigenvalue, the corresponding eigenvectors of eigenvalues  $\xi$  can be considered as in appendix A. Hence, the exact solutions of Eq. (29) can be expressed as:

$$N(x, q, s) = \sum_{i=1}^4 B_i Y_i e^{-\xi_i x} \quad (34)$$

Thus, the general solutions of the field variables can be given as functions of  $q, s$  and  $t$  as:

$$\bar{\theta}^*(x, q, p) = \sum_{i=1}^4 B_i T_i e^{-\xi_i x} \quad (35)$$

$$\bar{u}^*(x, q, p) = \sum_{i=1}^4 B_i u_i e^{-\xi_i x} \quad (36)$$

$$\bar{v}^*(x, q, p) = \sum_{i=1}^4 B_i v_i e^{-\xi_i x} \quad (37)$$

$$\bar{\varphi}^*(x, q, p) = \sum_{i=1}^4 B_i \varphi_i e^{-\xi_i x} \quad (38)$$

$$\bar{\sigma}_{xx}^*(x, q, p) = \sum_{i=1}^4 B_i (-\xi_i u_i + i q (1 - 2s_1) v_i + s_2 \varphi_i - s_3 T_i) e^{-\xi_i x} \quad (39)$$

$$\bar{\sigma}_{xy}^*(x, q, p) = \sum_{i=1}^4 B_i s_1 (-\xi_i v_i + i q u_i) e^{-\xi_i x} \quad (40)$$

where  $B_1, B_2, B_3$  and  $B_4$  are constants which can be calculated by using the problem boundary conditions such that the terms containing exponentials of increasing nature in the spatial variable  $x$  have been discarded due to the regularity conditions of the solutions at infinity, while  $u_i, v_i, T_i$  and  $\varphi_i$  are the components of corresponding eigenvector. Now, for any function  $\bar{M}^*(x, q, s)$ , Fourier transforms inverse can be written as

$$\bar{M}(x, y, s) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \bar{M}^*(x, q, s) e^{iqy} dq \quad (41)$$

Finally, to get the general solutions of the displacements components, temperature increment, the stress components and the change in volume fraction field of voids distributions along the distances  $x, y$  at any time  $t$ , Stehfest Stehfest (1970) numerical inversion approach has been chosen. In this approach, the Laplace transforms inverse for  $\bar{M}(x, y, s)$  are approximated by

$$M(x, y, t) = \frac{\ln(2)}{t} \sum_{n=1}^N V_n \bar{M}\left(x, y, n \frac{\ln(2)}{t}\right) \quad (42)$$

where

$$V_n = (-1)^{\left(\frac{N}{2}+1\right)} \sum_{p=\frac{n+1}{2}}^{\min\left(n, \frac{N}{2}\right)} \frac{(2p)! p^{\left(\frac{N}{2}+1\right)}}{p! (n-p)! \left(\frac{N}{2}-p\right)! (2n-1)!} \quad (43)$$

where  $N$  is the term numbers.

#### 4. Results and discussion

For numerical computations, magnesium medium was chosen for purposes of numerical calculations. The values of parameters can be taken as in Othman and Marin (2017)

$$\zeta_1 = 1.475 \times 10^{10} (N) (m^{-2}), \alpha = 3.688 \times 10^{-5} (N), \omega_0 = 0.0787 \times 10^{-3} (N) (m^{-2}) (s^{-1}),$$

$$\alpha_t = 1.98 \times 10^{-6} (k^{-1}), K = 1.7 (W) (m^{-1}) (k^{-1}), \beta = 2.68 \times 10^6 (N) (m^{-2}) (k^{-1}),$$

$$T_0 = 298 (K), c_e = 1040 (J) (kg^{-1}) (K^{-1}), \psi = 1.753 \times 10^{-15} (m^2), a = 0.25,$$

$$\mu = 3.278 \times 10^{10} (N) (m^{-2}), \lambda = 2.17 \times 10^{10} (N) (m^{-2}), \rho = 1740 (kg) (m^{-3}),$$

$$m = 2 \times 10^6 (N) (m^{-2}) (k^{-1}), b = 1.13840 \times 10^{10} (N) (m^{-2}), t = 0.6.$$

The above data have been applied to study the fractional order thermoelastic wave assessment in a two-dimensional porous material by the eigenvalue approach. The change in volume fraction field of voids distribution  $\varphi$ , the displacement components  $u, v$ , the stress components  $\sigma_{xx}$ ,  $\sigma_{xy}$  and the variations of temperature  $\Theta$ , are studied. The material is considered to be an isotropic and homogeneous

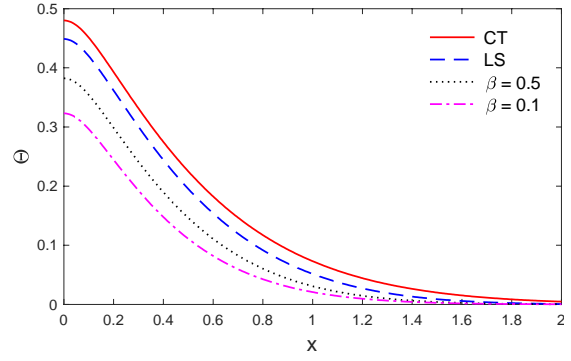


Fig. 1 The variations of temperature  $\Theta$  versus  $x$  when  $y = 0.5$  for different values of the fractional-order parameter  $\beta$

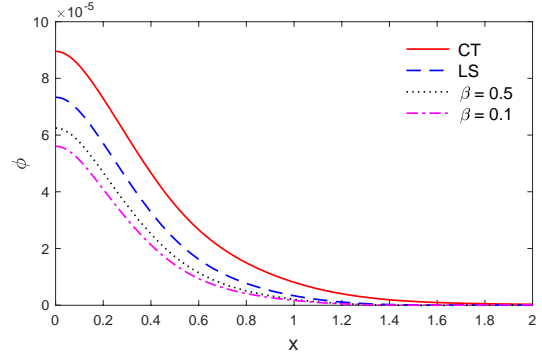


Fig. 2 The changes in volume fraction field of voids distributions  $\varphi$  versus  $x$  when  $y = 0.5$  for different values of the fractional-order parameter  $\beta$

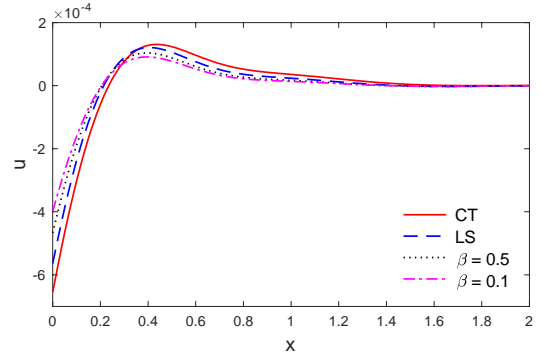


Fig. 3 The variations of horizontal displacement  $u$  versus  $x$  when  $y = 0.5$  for different values of the fractional-order parameter  $\beta$

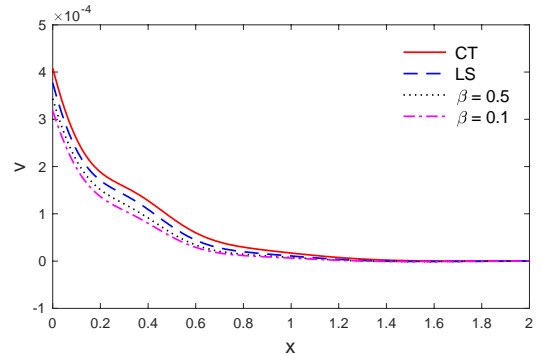


Fig. 4 The variations of vertical displacement  $v$  versus  $x$  when  $y = 0.5$  for different values of the fractional-order parameter  $\beta$

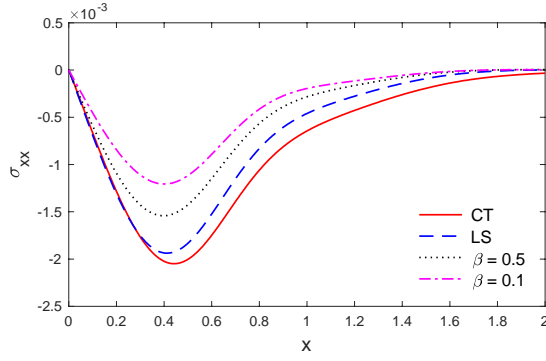


Fig. 5 The variations of stress  $\sigma_{xx}$  versus  $x$  when  $y=0.5$  for different values of the fractional-order parameter  $\beta$

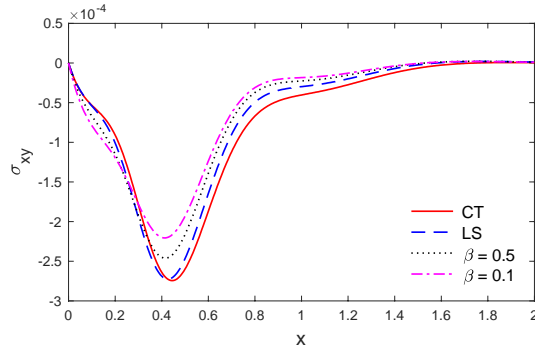


Fig. 6 The variations of stress  $\sigma_{xy}$  versus  $x$  when  $y=0.5$  for different values of the fractional-order parameter  $\beta$

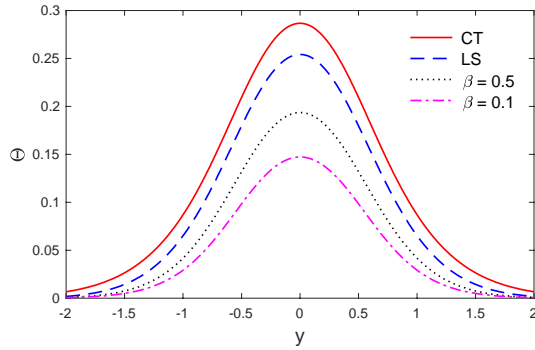


Fig. 7 The variations of temperature  $\Theta$  versus  $y$  when  $x=0.5$  for different values of the fractional-order parameter  $\beta$

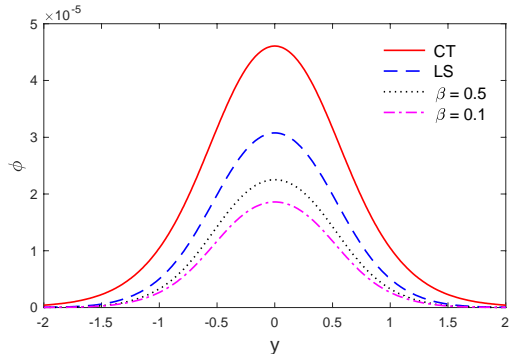


Fig. 8 The changes in volume fraction field of voids distributions  $\phi$  versus  $y$  when  $x=0.5$  for different values of the fractional-order parameter  $\beta$

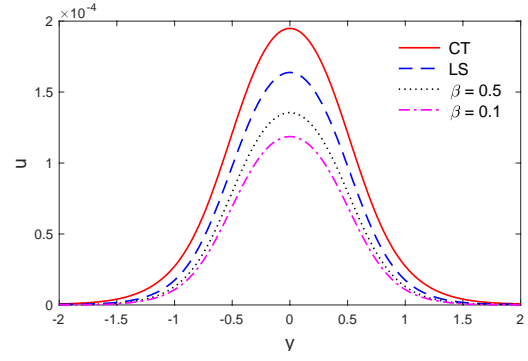


Fig. 9 The variations of horizontal displacement  $u$  versus  $y$  when  $x=0.5$  for different values of the fractional-order parameter  $\beta$

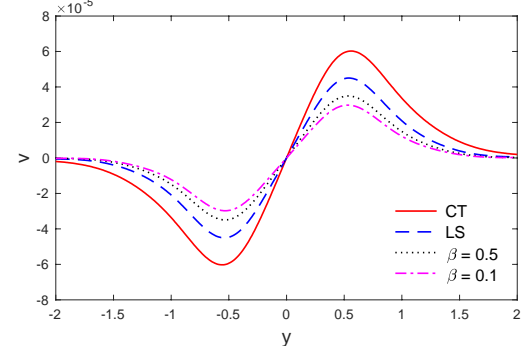


Fig. 10 The variations of vertical displacement  $v$  versus  $y$  when  $x=0.5$  for different values of the fractional-order parameter  $\beta$

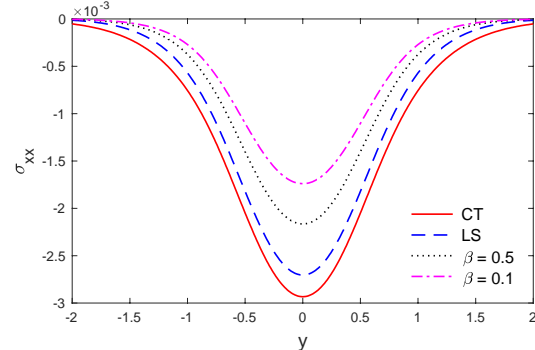


Fig. 11 The variations of stress  $\sigma_{xx}$  versus  $y$  when  $x=0.5$  for different values of the fractional-order parameter  $\beta$

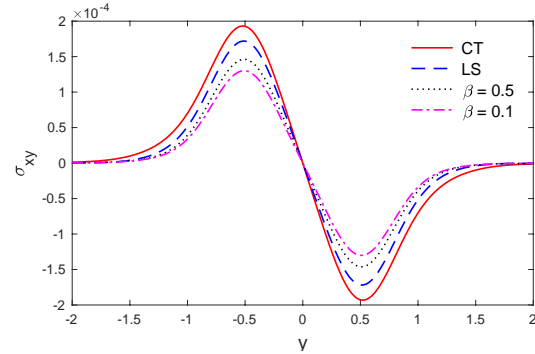


Fig. 12 The variations of stress  $\sigma_{xy}$  versus  $y$  when  $x=0.5$  for different values of the fractional-order parameter  $\beta$

two-dimensional medium. Fig. 1 shows the variations of temperature with respect to the distance  $x$ . It is observed that it begins from maximum value according to the application of boundary condition and decreases with the increasing  $x$  to reach to zero. Fig. 2 depicts the change in volume fraction field of voids distributions  $\varphi$  with respect to the distances  $x$ . It is noticed that it decreases with the increasing  $x$  till attaining zero. Fig. 3 predicts the variations of horizontal displacement  $u$  versus  $x$ . It is observed that it attains maximum negative values and gradually increases until it attains peak values and then decreases to close to zero. Fig. 4 displays the variations of vertical displacement versus  $x$  which have maximums values on  $x = 0$  and decreases with the increasing  $x$ . Figs. 5 and 6 predict the stress components variations  $\sigma_{xx}$  and  $\sigma_{xy}$  along  $x$ . It is observed that the stress magnitudes, always started from zero which satisfied the boundary conditions. Figs. 7 and 8 show the variation of temperature  $\theta$  and the variation of change in volume fraction field of voids  $\varphi$  versus the distance  $y$  when  $x = 0.5$ . It is observed that they have maximum values at the length of thermal surface ( $|y| \leq 0.5$ ) then start to reduce just near the edge ( $|y| \leq 0.5$ ) where they decrease and finally close to zero values. Figure 9 display the variation of horizontal displacement  $u$  versus the distance  $y$ . It is observed that it has maximum value at the length of the heating surface ( $|y| \leq 0.5$ ), and it starts to reduce just near the edge ( $y = \pm 0.5$ ), and after that decreases to zero values. Fig. 10 shows the variation of vertical displacement  $v$  versus the distance  $y$ . It indicates that the vertical displacement starts raising at the beginning and ending of the thermal surface ( $|y| \leq 0.5$ ), and has small values at the middle of the thermal surface, then it starts increasing and come to maximum values just near the edge ( $y = \pm 0.5$ ), after that it decreases to reach to zero. The components of stress  $\sigma_{xx}$  and  $\sigma_{xy}$  versus  $y$  are shown in Figs. 11 and 12.

Finally, Figs. 2 to 12 show the variations of all physical quantities with respect to the distance  $x$  and the distance  $y$  at  $t = 0.5$ . These figures display the predict curves under various theories of thermo-elasticity. In these figures, the classical dynamically coupled theory (CT) appeared in solid lines, the Lord and Shulman (LS) theory appeared in dashed lines while the other curves that refer to the generalized thermoelastic theory under fractional time derivative ( $\beta = 0.5, \beta = 0.1$ ). As expected, it can be found that the fractional derivative parameter  $\beta$  have the major impact on the values of all the studied fields.

## 5. Conclusions

Based on the generalized thermoelastic theory with fractional derivative, the variations of temperature, the components of displacement, the components of stress and the changes in volume fraction field in a two-dimension porous medium are studied. The non-dimensional resulting has been solved employing the and Fourier and Laplace transforms technique and has been solved using the eigenvalue method. The great effects of the fractional

derivative parameter are discussed for all physical quantities.

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IC



## Appendix A

$$f_1 = a_{51}a_{64}a_{72}a_{83} + a_{51}a_{62}a_{73}a_{84} - a_{51}a_{64}a_{73}a_{82} + a_{51}a_{63}a_{74}a_{82} - a_{51}a_{62}a_{74}a_{83} - a_{51}a_{63}a_{72}a_{84}.$$

$$f_2 = a_{56}a_{64}a_{73}a_{85} + a_{56}a_{65}a_{74}a_{83} + a_{57}a_{62}a_{74}a_{85} - a_{56}a_{63}a_{74}a_{85} + a_{51}a_{63}a_{72} - a_{51}a_{73}a_{84} - a_{62}a_{73}a_{84} - a_{56}a_{65}a_{73}a_{84} - a_{63}a_{74}a_{82} - a_{57}a_{62}a_{75}a_{84} + a_{58}a_{62}a_{75}a_{83} - a_{56}a_{64}a_{75}a_{83} - a_{51}a_{62}a_{84} + a_{63}a_{72}a_{84} - a_{51}a_{62}a_{73} - a_{58}a_{63}a_{75}a_{82} + a_{57}a_{64}a_{75}a_{82} - a_{58}a_{65}a_{72}a_{83} + a_{51}a_{64}a_{82} + a_{64}a_{73}a_{82} + a_{58}a_{65}a_{73}a_{82} + a_{51}a_{74}a_{83} + a_{62}a_{74}a_{83} - a_{57}a_{65}a_{74}a_{82} - a_{64}a_{72}a_{83} + a_{57}a_{65}a_{72}a_{84} + a_{56}a_{63}a_{75}a_{84} + a_{58}a_{63}a_{72}a_{85} - a_{57}a_{64}a_{72}a_{85} - a_{58}a_{62}a_{73}a_{85},$$

$$f_3 = a_{51}a_{73} - a_{64}a_{82} - a_{58}a_{65}a_{82} - a_{74}a_{83} - a_{58}a_{75}a_{83} + a_{58}a_{62}a_{85} - a_{56}a_{64}a_{85} + a_{58}a_{73}a_{85} - a_{57}a_{74}a_{85} + a_{51}a_{84} + a_{62}a_{84} + a_{56}a_{65}a_{84} + a_{73}a_{84} + a_{57}a_{75}a_{84} + a_{62}a_{73} + a_{56}a_{65}a_{73} + a_{57}a_{62}a_{75} - a_{56}a_{63}a_{75} + a_{51}a_{62} - a_{63}a_{72} - a_{57}a_{65}a_{72},$$

$$f_4 = a_{51} + a_{62} + a_{65}a_{56} + a_{75}a_{57} + a_{84} + a_{85}a_{58} + a_{73}.$$

## Appendix B

$$Y_5 = Y_1\xi, Y_6 = Y_2\xi, Y_7 = Y_3\xi, Y_8 = Y_4\xi,$$

$$Y_1 = -(\xi a_{58}(a_{62} - \xi^2) - \xi a_{56}a_{64})(\xi(a_{73} - \xi^2)a_{58} - a_{57}a_{74}\xi) + \xi^2(a_{58}a_{63} - a_{57}a_{64})(a_{58}a_{72} - a_{56}a_{74}),$$

$$Y_2 = -\xi(a_{63}a_{58} - a_{64}a_{57})(a_{74}(\xi^2 - a_{51}) + \xi^2a_{75}a_{58}) - \xi(a_{64}(\xi^2 - a_{51}) + a_{65}a_{58}\xi^2)((\xi^2 - a_{73})a_{58} + a_{74}a_{57}),$$

$$Y_3 = a_{64}(\xi^2a_{56}a_{75} + a_{72}(\xi^2 - a_{51})) + \xi^2a_{58}(a_{72}a_{65} + a_{75}(\xi^2 - a_{62})) - a_{58}\xi(((\xi^2 - a_{51})(\xi^2 - a_{62}) - a_{65}a_{56}\xi^2)a_{74},$$

$$Y_4 = -a_{58}\xi(\xi^6 + a_{51}((\xi^2 - a_{73})a_{62} - \xi^4 + a_{72}a_{63} + a_{73}\xi^2) - \xi^2((a_{65}a_{57} + a_{63})a_{72} + (a_{73} + a_{75}a_{57})\xi^2 + a_{56}(a_{65}(\xi^2 - a_{73}) + a_{63}a_{75}) + a_{62}(\xi^2 - a_{73} - a_{57}a_{75}))).$$